ASX Announcement
20 August 2026

PLS RESOURCES AND RESERVES RE-REPORTED TO JORC CODE

Paladin Energy Ltd (ASX:PDN, TSX:PDN, OTCQX:PALAF) ("**Paladin**" or the "**Company**") is pleased to present its Mineral Resource and Ore Reserve estimates for the Patterson Lake South ("**PLS**") project in accordance with the JORC Code (2012), offering an alternative from prior and on-going disclosure under NI 43-101.

The estimates were previously reported in the Company's 2025 Annual Report as a foreign estimate under NI 43-101. This announcement re-reports those estimates in accordance with JORC to align with ASX Listing Rules and establish a consistent basis for future reporting.

Key Points

- There is no material change to the previously disclosed PLS mineral resource and mineral/ore reserve estimates as a result of re-reporting those estimates in accordance with the JORC Code. The Mineral Resource incorporates subsequent non-material updates to the R840W and R1515W zones, while the Mineral/Ore Reserve remains unchanged.
- The estimates have been re-reported using the same underlying data, geological interpretation, mine design and modifying factors that support the previously disclosed foreign estimates using Canadian Institute of Mining, Metallurgy and Petroleum (CIM) standards applicable under NI 43-101, with subsequent non-material Mineral Resource updates incorporated where applicable.
- Establishes a clear JORC baseline for all future ASX disclosures

As a dual-listed entity, the Company has previously reported Mineral Resource and Mineral/Ore Reserve estimates for the PLS Project in accordance with NI 43-101 for Canadian regulatory purposes. The Company will continue to report using JORC and CIM standards in compliance with NI 43-101. JORC code is an acceptable reporting code under NI 43-101 and is consistent with CIM. The confidence categories between CIM and JORC are the same, and therefore there is no requirement for modification of the confidence categories. The Mineral Resource and Ore Reserve estimates have now been:

- reviewed against JORC Code (2012) requirements
- confirmed as appropriate in classification and supporting assumptions
- re-reported in JORC format without material modification

The Company considers the methodologies underpinning the Mineral Resource and Ore Reserve estimates for the PLS Project, including geological interpretation, estimation methodology, mining assumptions and modifying factors, to be substantially equivalent to those previously reported under NI 43-101.

The Mineral Resource estimate is based on the same drilling, sampling, QA/QC and geological interpretation previously disclosed and has not been re-estimated. Figure 1 shows drillhole collar locations and Figure 2 shows a long section across the Triple R deposit. The Mineral Resource estimate reported in this announcement includes subsequent non-material Mineral Resource updates for the R840W and R1515W zones.

The Ore Reserve estimate is based on the 17 May 2022 NI 43-101 mineral resource estimate and the Feasibility Study mine design and modifying factors for the PLS Project with an effective date of 17 January 2023. The non-material R1515W Mineral Resource update from 30 June 2025 is not included in the reported Ore Reserve. The Ore Reserve estimate is derived from the Mineral Resource and incorporates the same mining, metallurgical, economic and other modifying factors, including mine design and production assumptions, as previously reported.

Future Reporting

This release establishes a JORC-compliant reference point for both Mineral Resources and Ore Reserves for the PLS Project.

Going forward, the Company will:

- report in accordance with the JORC Code (2012) for ASX disclosures; and
- reduce the need for cross-referencing between NI 43-101 and JORC in future ASX reporting, including the upcoming Annual Report. NI 43-101 disclosure will continue to be maintained for Canadian filings as required.

Mineral Resources

		Mt	Grade % U_3O_8	Grade g/t Au	Mlb U_3O_8	Koz Au
Indicated	Triple R	2.9	1.88	0.59	118.8	54.4
Inferred	Triple R	0.4	1.19	0.46	10.9	6.1
Total		**3.3**	**1.80**	**0.57**	**129.7**	**60.5**

Mineral Resources are reported as at 30 June 2025, reflecting the inclusion of the non-material R1515W Mineral Resource update, and are reported inclusive of Ore Reserves. Mineral Resources are reported above an underground cut-off grade of 0.25% U_3O_8, based on a long-term uranium price assumption of US$50/lb U_3O_8, cost estimates derived during the PLS Pre-Feasibility Study, a metallurgical recovery assumption of 95%. Gold is reported as a by-product Mineral Resource associated with the Triple R uranium mineralisation. The Mineral Resource assumes potential extraction by conventional underground mining methods; no mining dilution has been applied to the Mineral Resource estimate. Tonnages are estimated on a dry basis. Figures are rounded to reflect appropriate precision and totals may not add due to rounding.

Ore Reserves

		Mt	Grade % U_3O_8	Mlb U_3O_8
Probable	R780E Zone	2.6	1.46	84.8
	R00E Zone	0.1	1.24	1.5
	R840W Zone	0.3	1.04	7.4
Total		**3.0**	**1.41**	**93.7**

Ore Reserves are derived from the Triple R Mineral Resource estimate with an effective date of 17 May 2022 and are based on the PLS Feasibility Study, which has an effective date of 17 January 2023. Ore Reserves are reported above a 0.25% U_3O_8 cut-off grade and are based on a uranium price assumption of US$65/lb U_3O_8. Metallurgical assumptions include high uranium recovery supported by Feasibility-level test work, including 98.4% average uranium extraction in leach testing, with the cut-off grade based on a 97% metallurgical recovery assumption. Mining assumptions include longhole stoping and drift-and-fill mining, with net dilution of 24%, 95% mining recovery applied to stopes and 100% extraction assumed for development mining. No gold Ore Reserve is reported in this announcement. Figures are rounded to reflect appropriate precision and totals may not add due to rounding.

Mineral Resource Summary

The Triple R deposit is a basement-hosted, unconformity-related uranium deposit located on the southwest margin of the Athabasca Basin in Saskatchewan, Canada. Mineralisation occurs principally within structurally controlled zones hosted in metamorphic basement rocks underlying Patterson Lake and remains open in several areas along the broader mineralised corridor.

The Mineral Resource estimate has been prepared using drilling, geological interpretation, density and assay data collected by Fission Uranium Corp. (prior to its acquisition by Paladin in 2024) and subsequently reviewed by Paladin. The estimate includes the R1515W, R840W, R00E, R780E and R1620E mineralised zones that collectively comprise the Triple R deposit.

The estimate is based on 542 drillholes comprising geological, geotechnical and geochemical information supported by a comprehensive quality assurance and quality control program including the routine insertion of certified reference materials, blanks and duplicate samples. Independent check assaying and database validation were undertaken and no material issues were identified that would adversely affect the integrity of the Mineral Resource estimate.

Geological wireframes were constructed to constrain mineralised domains and uranium grades were estimated using inverse distance cubed interpolation within constrained estimation domains. Resource blocks were classified as Indicated or Inferred based primarily on drill spacing, geological continuity and estimation confidence.

Mineral Resources are reported above a cut-off grade of 0.25% U_3O_8. The cut-off grade was derived using a long-term uranium price assumption of US$50/lb U_3O_8, estimated underground mining costs, metallurgical recovery assumptions of 95% and other operating cost and revenue parameters appropriate for a potential underground mining operation.

Bulk density was estimated using more than 15,000 density measurements collected throughout the deposit and interpolated independently from uranium grades.

The Competent Person considers that the Mineral Resource has reasonable prospects for eventual economic extraction through conventional underground mining methods. Mineral Resources are reported inclusive of Ore Reserves.

The Mineral Resource has been classified as Indicated and Inferred Mineral Resources based on drill spacing, geological continuity, grade continuity and estimation confidence. No Measured Mineral Resources are reported. Given the planned underground mining method and the compact, high-grade nature of the deposit, the Company considers it more appropriate to complete additional close-spaced underground drilling from development workings to support future Measured Mineral Resource classification. This approach is expected to provide a more cost-effective means of achieving the higher confidence levels required for Measured Mineral Resources than would be obtained through additional surface drilling alone. The Competent Person considers the reported classification appropriately reflects the available data and the confidence in the estimate.

The Mineral Resource estimate reported in this announcement incorporates subsequent non-material updates to the R840W and R1515W zones completed after the effective date of the May 2022 Mineral Resource estimate. These updates do not materially alter the overall geological interpretation, classification or economic outlook of the deposit.

Ore Reserve Summary

The Ore Reserve estimate is based on the Triple R Mineral Resource estimate with an effective date of 17 May 2022 and is supported by the Feasibility Study for the PLS project with an effective date of 17 January 2023. Subsequent updates to the R840W and R1515W Mineral Resources have not yet been incorporated into mine design or reserve conversion studies and therefore are not reflected in the reported Ore Reserve.

Ore Reserves have been derived from Indicated Mineral Resources through detailed mine design, mine scheduling and application of modifying factors consistent with JORC Code requirements. Approximately 84% of the Indicated Mineral Resource within the mining areas was converted to Probable Ore Reserves following application of modifying factors.

Mining is proposed as an underground operation using a combination of longitudinal longhole stoping and drift-and-fill mining. Longhole stoping represents the primary mining method, while drift-and-fill mining is applied in crown pillar areas where geotechnical conditions require a more selective mining approach.

Mineable stope shapes were generated using Datamine Mineable Shape Optimiser and subsequently refined through detailed engineering design and scheduling. Mining assumptions include:

- 95% mining recovery for longhole stopes;
- Average net dilution of approximately 24%;
- Minimum mining width of 4 metres for longhole stoping;
- Additional dilution allowances for backfill exposure and proximity to geological contacts; and
- Exclusion of Inferred Mineral Resources from Ore Reserve estimation.

The Ore Reserve is reported above a cut-off grade of 0.25% U_3O_8 and is based on a long-term uranium price assumption of US$65/lb U_3O_8.

Metallurgical assumptions are supported by extensive laboratory testing completed as part of the Feasibility Study. Test-work demonstrated high uranium recoveries across representative lithologies and grades, including average uranium extraction of approximately 98.4% during feasibility-level test-work. The process flowsheet comprises conventional grinding, acid leaching, solvent extraction and yellowcake production technology consistent with established Athabasca Basin uranium operations.

The Feasibility Study outlines a 1,000 t/d underground mining and processing operation producing marketable uranium concentrate. Life-of-mine average mill feed grade is estimated at approximately 1.41% U_3O_8 with forecast overall uranium recovery of approximately 97%.

Material risks to the Ore Reserve include permitting timelines, uranium price assumptions, geotechnical performance, groundwater management and execution of the planned underground mining method; however, these risks were considered in the Feasibility Study and are not considered sufficient to materially undermine the Ore Reserve estimate.

Infrastructure, Environmental and Economic Considerations

The Ore Reserve is supported by a completed Feasibility Study demonstrating the technical and economic viability of the PLS project.

The study incorporates:

- Initial capital cost estimate of approximately C$1.16 billion;
- Life-of-mine sustaining capital of approximately C$384 million;
- Average operating costs of approximately C$13.02/lb U_3O_8 produced;
- Post-tax NPV8 of approximately C$1.2 billion; and
- Post-tax IRR of approximately 27%.

The PLS project benefits from access via Saskatchewan Highway 955 and sufficient land tenure to support planned mine, process plant, tailings management and supporting infrastructure.

Environmental assessment studies have been completed and Saskatchewan Ministerial Approval for the Environmental Impact Statement was received in February 2026. Ongoing permitting activities are progressing in accordance with regulatory requirements.

The Company considers there are reasonable grounds to expect that all material permits, approvals and licences required for Project development can be obtained within the timeframes contemplated by the Feasibility Study. No material unresolved environmental, social, tenure or other matters have been identified that are expected to materially impact extraction of the reported Ore Reserve.

This announcement has been authorised for release by the Board of Directors.

Contacts

Investor Relations

Paula Raffo

T: +61 8 9423 8100
E: paula.raffo@paladinenergy.com.au

Media

Anthony Hasluck

T: +61 438 522 194
E: anthony.hasluck@paladinenergy.com.au

Competent Person's Statement

The Mineral Resources contained in this document is based on, and fairly represents, information and supporting documentation prepared by Mr Kanan Sarioglu, VP Exploration of Paladin Canada Inc. (formerly Fission Uranium Corp.) a wholly-owned subsidiary of Paladin, who is a registered Professional Geoscientist (P.Geo) with the Engineers and Geoscientists of British Columbia (EGBC), the Association of Professional Engineers and Geoscientists of Alberta (APEGA) and the Association of Professional Engineers and Geoscientists of Saskatchewan (APEGS). Mr Sarioglu has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity undertaken, to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves and is a Qualified Person as defined by Canadian National Instrument NI 43-101. Uranium Ore Reserves for the PLS project included in this document were derived from the Technical report titled "Feasibility Study, NI 43-101 Technical Report, for PLS Property" (effective date 17 January 2023), prepared in accordance with NI 43-101 and available on www.sedarplus.ca. Indicated and Inferred Mineral Resource totals presented in this document differ from the aforementioned technical report due to an updated Mineral Resource estimates at the R840W zone in May 2023 and the R1515W zone in June 2025, which are considered non-material. Mr Sarioglu consents to the inclusion of the estimates of Mineral Resources and Ore Reserves, and the relevant supporting information, in the form and context in which it appears.

The Ore Reserves contained in this document has been reviewed and approved by Lewis Kitchen, Principal Mining Consultant, Mining Plus Canada Consulting Ltd, who is a registered Professional Engineer (P.Eng.) with Engineers and Geoscientists of BC (Registration #50164). Mr Kitchen has sufficient experience which is relevant to the style of mineralisation and type of deposit under consideration and to the activity undertaken, to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves and is a Qualified Person as defined by Canadian National Instrument NI 43-101. Uranium Ore Reserves for the PLS project included in this document were derived from the Technical report titled "Feasibility Study, NI 43-101 Technical Report, for PLS Property" (effective date 17 January 2023), prepared in accordance with NI 43-101 and available on www.sedarplus.ca. Mr Kitchen consents to the inclusion of the estimates of Mineral Resources and Ore Reserves, and the relevant supporting information, in the form and context in which it appears.

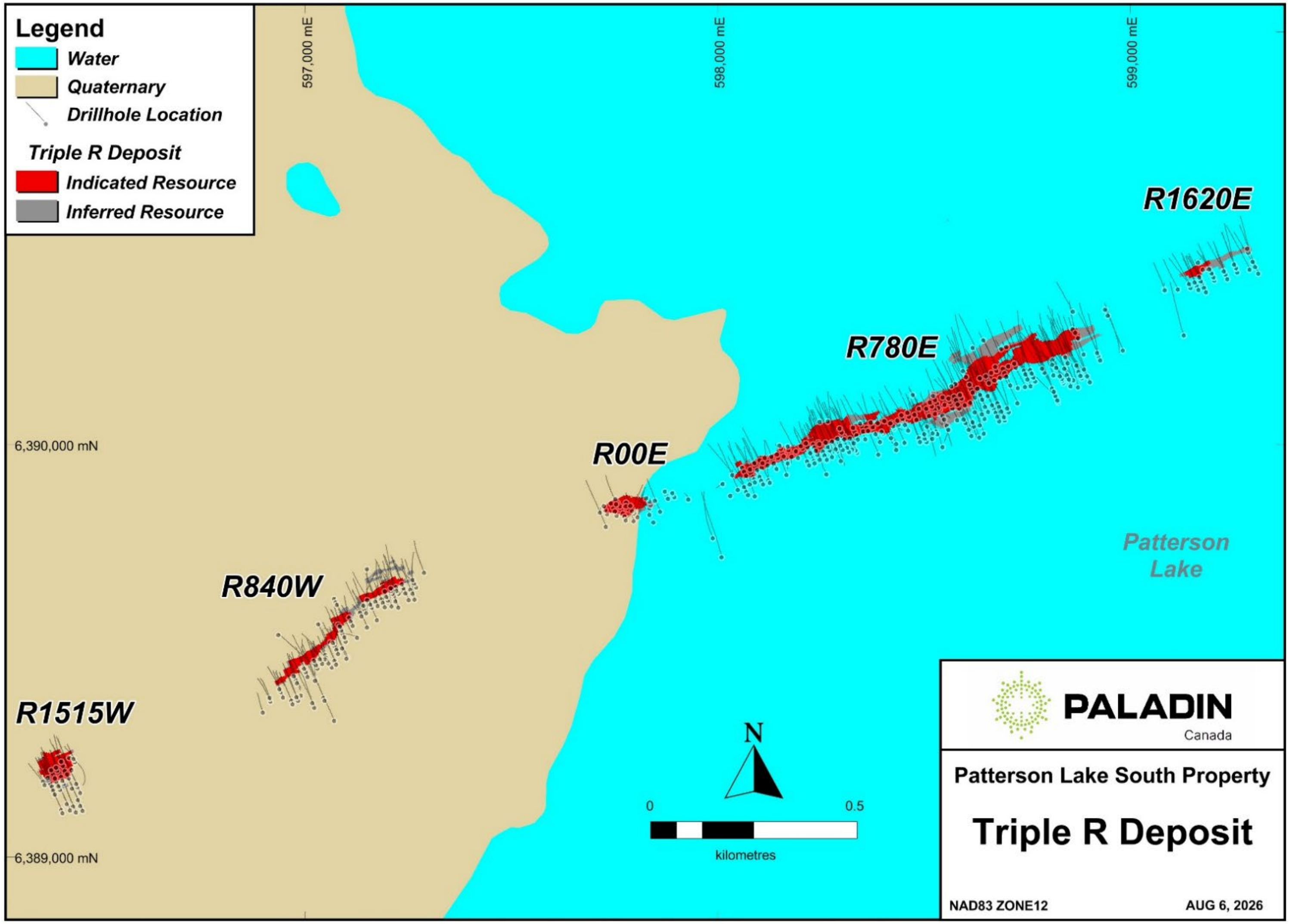

Figure 1: Plan Map of Patterson Lake South Project: Triple R Resources

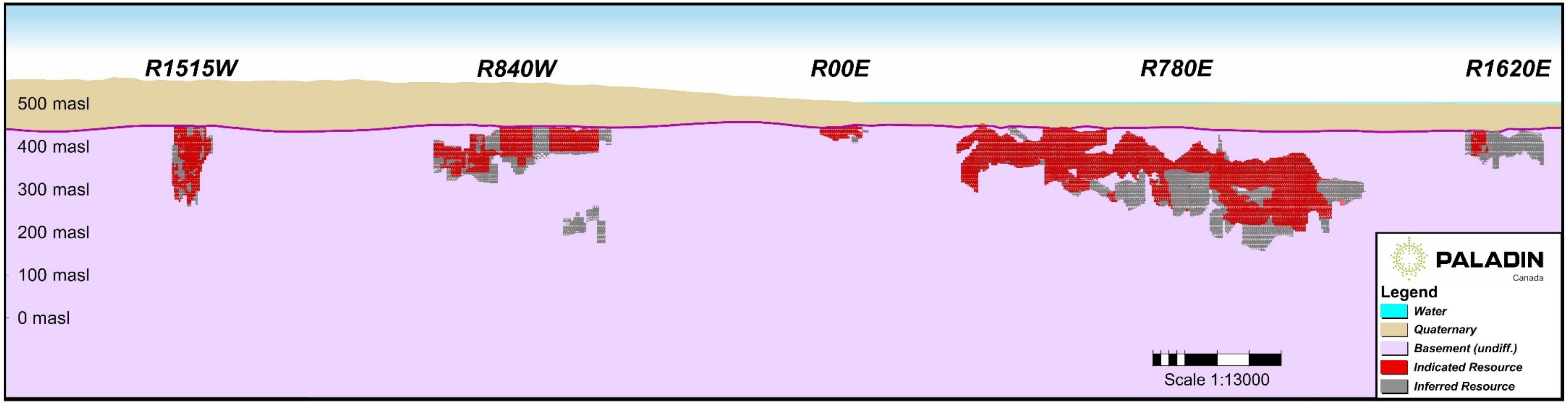

Figure 2: Long Section of Patterson Lake South Project: Triple R Resources

JORC Code, 2012 Edition – Table 1

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	• *Nature and quality of sampling (e.g. cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling.* • *Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used.* • *Aspects of the determination of mineralisation that are Material to the Public Report.* • *In cases where 'industry standard' work has been done this would be relatively simple (e.g. 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases, more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (e.g. submarine nodules) may warrant disclosure of detailed information.*	• Drilling related to the PLS project / Triple R deposit was carried out using a coring rig. Drill core that returned handheld RS-121 scintillometer readings equal to or greater than 300 counts per second (cps) was marked for sampling and split in half along the core axis into 50 cm core-length samples. One half of the core was placed into a labelled sample bag and sent for geochemical analysis and weight percent (wt%) U_3O_8 assay, while the other half remained in the core box as a permanent record. Core samples for geochemistry and U_3O_8 assay were crushed to 60% passing −2 mm, and a 100 g to 200 g sub-sample was split using a riffle splitter. The sub-sample was then pulverized to 90% passing 106 μm using a standard puck-and-ring grinding mill. An aliquot of the pulp was digested in a concentrated mixture of HNO_3:HCl in a hot water bath for one hour and was then diluted with de-ionized water. The samples were analysed using a Perkin Elmer ICP-OES instrument.
Drilling techniques	• *Drill type (e.g. core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (e.g. core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).*	• The type of drill used at Triple R was a Zinex Mining Corp. A5 coring rig or equivalent. All drillholes were NQ diameter (47.6 mm), standard tube. A limited number of drillholes with poor ground conditions near the top of bedrock utilized HQ (63.5 mm) diameter coring until competent rock was cored, after which NQ coring continued to the end of the hole. In rare occasions where the NQ drill rods became stuck due to ground conditions, BQ diameter (36.4 mm) coring was performed to continue the drillhole. Beginning in January 2013, a reverse circulation or sonic drill was used to set 4 ¾ inch casing through the overburden and into shallow bedrock at Triple R prior to diamond drilling.

Criteria	JORC Code explanation	Commentary
		• From October to November 2012, 12 4.5 inch (11.43 cm) diameter dual rotary drill holes totalling 1,548 m were completed by J.R. Drilling Ltd. of Cranbrook, British Columbia, using a Foremost DR-12 drill. • Drill core was oriented using a REFLEX ACTIII from 2014 onwards. • Select drillholes across Triple R also had downhole acoustic televiewer (ATV) coverage.
Drill sample recovery	• *Method of recording and assessing core and chip sample recoveries and results assessed.* • *Measures taken to maximise sample recovery and ensure representative nature of the samples.* • *Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.*	• Drill core from Triple R was logged geotechnically on a run-by-run or ISRM rock strength basis and included the number of naturally occurring fractures, mechanical fractures, intact core recovery, rock quality designation (RQD), ISRM rock strength, longest stick, and radioactivity measured in cps. • Core recovery at Triple R was generally very good, which allowed representative samples to be taken and accurate analyses to be performed. • Radioactivity was confirmed in areas of poor core recovery using a downhole gamma probe. • No sampling bias was observed due to preferential loss or gain of drill core
Logging	• *Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.* • *Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.* • *The total length and percentage of the relevant intersections logged.*	• All drill core was descriptively logged by a Paladin Canada Inc. geologist, with particular attention given to major and minor lithologies, alteration, structure, and uranium mineralization. • Paladin Canada Inc. geotechnicians recorded drill core recovery, rock RQD, rock strength, longest stick, natural breaks, joint condition, weathering grade, discontinuity features, and radioactivity. • Logging and sampling information was entered into a spreadsheet-based template, which was reviewed at the end of the program and was then integrated into the project’s digital database. • All drill core was photographed while wet using a digital camera before sampling.

Criteria	JORC Code explanation	Commentary
		• Drill core was logged geologically and geotechnically in sufficient detail to support mining studies, metallurgical studies, and the Mineral Resource estimate.
Sub-sampling techniques and sample preparation	• *If core, whether cut or sawn and whether quarter, half or all core taken.* • *If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.* • *For all sample types, the nature, quality and appropriateness of the sample preparation technique.* • *Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.* • *Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.* • *Whether sample sizes are appropriate to the grain size of the material being sampled.*	• All core samples were standardized to half-meter lengths, except in zones of poor recovery (<25%) where the interval length was adjusted. • All core samples consisted of half-split NQ-sized drill core that was split parallel to the core axis, except in limited cases where BQ or HQ-sized coring was used. Half of the drill core from each sample interval was placed into a marked and tagged sample bag, while the remaining half was left in the core box as a permanent record. No subsampling was carried out. • Drill core was half-split using a manual core splitter, with efforts made to ensure consistent representativity. • At least two duplicate samples were collected from each mineralized drillhole, and in thicker zones of mineralization a duplicate was taken every 10 m throughout the zone. • Because drill core samples covered the full half-meter interval, they were considered appropriate in size relative to the material being sampled.
Quality of assay data and laboratory tests	• *The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.* • *For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.* • *Nature of quality control procedures adopted (e.g. standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.*	• Drill core samples were sent to the Saskatchewan Research Council (SRC) Geoanalytical Laboratory in Saskatoon, Saskatchewan, an SCC ISO/IEC 17025:2005 accredited facility. Uranium assay samples were analysed using the U_3O_8 wt% package, which was an ISO/IEC 17025 accredited method for determining U_3O_8 wt% in geological samples. For this package, an aliquot of sample pulp was digested in a concentrated $HCl:HNO_3$ mixture, the digest was diluted with deionized water, and the solution was analysed by ICP-OES. • The SRC Geoanalytical Laboratory inserted Certified Reference Material (CRM) samples for every 20 samples analysed and

Criteria	JORC Code explanation	Commentary
		performed duplicate analyses every 40 samples. SRC CRM and duplicate results were monitored by Paladin upon receipt. • Paladin's internal quality assurance–quality control program included the following components: • Determination of precision — was achieved through regular insertion of duplicate samples at each stage of the process where a sample was taken or split. • Determination of accuracy — was achieved through regular insertion of CRM samples. • Checks for contamination — were carried out through the insertion of blanks. • CRM were sourced from the Canadian Certified Reference Materials Project. UTS-3 (0.051% U_3O_8), RL-1 (0.201% U_3O_8), BL-5 (8.36% U_3O_8), and CUP-2 (88.92% U_3O_8), representing low-, medium-, high- and ultra-high-grade uranium references, respectively, along with a gold (CH-4) CRM, were inserted into the sample sequence for each drillhole that intersected >300 cps radioactivity on a handheld scintillometer. Blanks were also inserted into the sample sequence for these drillholes and were sourced from barren quartz veins intersected on the PLS property in historical drillholes. • Duplicate samples were taken at least twice per mineralized drillhole, or every 20 mineralized samples in thicker zones of mineralization and consisted of the remaining half-split core from the sample interval. • CRM, blanks, and duplicates made up approximately 5% of the total samples sent to the laboratory. • Uranium results for CRM and blanks were reviewed upon receipt from the laboratory. CRM failure criteria were triggered when a sample fell outside three standard deviations of the expected value, or when two consecutive samples fell outside two standard

Criteria	JORC Code explanation	Commentary
		deviations on the same side. Blank failure criteria were triggered when a sample returned a uranium concentration greater than five times the U_3O_8 assay detection limit. • In the event of a CRM or blank failure, the entire batch containing the failed CRM was reanalysed, and if the reanalysed batch passed, those sample values were used. • Coarse crushed or pulped reject material from 1,180 uranium assay samples was also sent to SGS Lakefield in Ontario, Canada, which acted as an umpire laboratory. • Umpire samples at SGS Lakefield were analysed using the GC_ICP14C package, which included leaching an aliquot of the sample pulp with an aqua regia mixture (3:1 $HCl:HNO_3$), followed by heating before the sample was analysed by ICP-OES/MS. • No significant discrepancies were identified between the SGS and SRC uranium assay results.
Verification of sampling and assaying	• *The verification of significant intersections by either independent or alternative company personnel.* • *The use of twinned holes.* • *Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.* • *Discuss any adjustment to assay data.*	• No drillholes were purposely twinned; however, scissor drillholes were completed to confirm uranium grades at the R780E and R840W zones. • All drillhole data was compiled and reviewed upon completion and was then imported and validated in Seequent MX Deposit and Bentley GEMS by Paladin staff. • Drillhole data was also reviewed by SLR personnel. • No uranium assay data was adjusted.
Location of data points	• *Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation.* • *Specification of the grid system used.* • *Quality and adequacy of topographic control.*	• All drillhole collars were positioned using a Trimble Real Time Kinematic (RTK) Global Positioning System (GPS), and all coordinates were recorded in UTM NAD83. A final collar position was collected using the Trimble RTK GPS once the drill had moved off the site. • Drillholes were aligned to the planned azimuth and dip using a TN-14

Criteria	JORC Code explanation	Commentary
		azimuth aligner. • Drillhole azimuth and dip information was measured every 50 m during drilling using a REFLEX EZ-Trac. Upon completion, drillholes were surveyed using a north-seeking gyro or equivalent tool, with readings taken every 10 to 25 m. • The PLS property had a detailed digital terrain model that provided topographic control.
Data spacing and distribution	• *Data spacing for reporting of Exploration Results.* • *Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied.* • *Whether sample compositing has been applied.*	• Not applicable as exploration results are not reported. • The sample spacing achieved is considered sufficient for the purposes Mineral Resource estimation and Ore Reserve reporting with the application of appropriate material classifications.
Orientation of data in relation to geological structure	• *Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.* • *If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.*	• Drillholes completed between 2012 and 2014 were predominantly drilled vertically due to two primary factors: 1) targeting anticipated sub-horizontal uranium mineralization near the top of metamorphic basement rock, and 2) operational constraints associated with drilling on Patterson Lake through thick overburden. Vertical orientations introduced a sampling bias, as these holes were subparallel to the basement lithology, which hosts the majority of the Triple R uranium mineralization, with the host rock dipping approximately 80° to the southeast. • Drilling conducted post-2014 adopted inclined drilling techniques with shallower dip angles. Drillholes were generally oriented perpendicular to the interpreted dip and dip direction of the basement rock, typically at 60–70° towards an azimuth of 333°, or as closely perpendicular to the basement rock as conditions allowed. • On selected drill lines, scissor holes were completed, oriented perpendicular to the typical southeast–northwest drilling trend, to validate the spatial orientation and continuity of the uranium mineralization.

Criteria	JORC Code explanation	Commentary
Sample security	• *The measures taken to ensure sample security.*	• Drill core samples were stored in tamper-proof pails with locking lids at the PLS core logging facility until shipment. Sample pails were counted and loaded onto a transport truck for shipment, accompanied by Dangerous Goods paperwork that outlined the number of pails and the total radioactivity of the shipment. Pail numbers and samples were verified by the SRC upon arrival. A strict chain of custody was maintained for transporting radioactive sample pails from PLS to the SRC.
Audits or reviews	• *The results of any audits or reviews of sampling techniques and data.*	• Sampling methods, chain of custody procedures, analytical techniques were reviewed and determined to be appropriate and meet acceptable industry standards.

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	• *Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.* • *The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.*	• The PLS project consists of 17 contiguous mineral dispositions (or mineral claims) outlined in the table below, covering an area of 31,039 ha which are located 630 km northwest of Saskatoon, Saskatchewan. The Triple R deposit is located on disposition S-111376.

Disposition ID	Good Standing Date
S-110707	25-Jun-2041
S-110955	28-Aug-2041
S-111375	10-Sep-2041
S-111376	10-Sep-2046
S-111377	10-Sep-2046
S-111783	28-Jul-2044
S-112217	11-Mar-2040
S-112218	11-Mar-2046
S-112219	11-Mar-2046

Criteria	JORC Code explanation	Commentary
		S-112220 – 11-Mar-2046 S-112221 – 11-Mar-2046 S-112222 – 11-Mar-2046 S-112282 – 19-Sep-2046 S-112283 – 19-Sep-2040 S-112284 – 19-Sep-2046 S-112285 – 19-Sep-2046 S-112370 – 20-Feb-2040 All mineral claims are 100% owned by Paladin Canada Inc. and are in good standing until the dates indicated above. • There are no material agreements on the PLS mineral claims.
Exploration done by other parties	• *Acknowledgment and appraisal of exploration by other parties.*	• The PLS project had been explored intermittently from the mid-to-late 1970s through to the present. The majority of historical drilling and relevant exploration work was carried out between 2011 and 2024 by Fission Uranium Corp. (prior to its acquisition by Paladin), and most recently, from 2025 onwards, by Paladin. All exploration work undertaken by Fission Uranium Corp. prior to its acquisition by Paladin was considered to have been completed to a very high standard.
Geology	• *Deposit type, geological setting and style of mineralisation.*	• Triple R is considered a basement hosted, high-grade, unconformity-related style uranium deposit.
Drill hole Information	• *A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:* ○ *easting and northing of the drill hole collar* ○ *elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar* ○ *dip and azimuth of the hole* ○ *down hole length and interception depth* ○ *hole length.* • *If the exclusion of this information is justified on the basis that the*	• Material drillhole information is provided in Appendix I.

Criteria	JORC Code explanation	Commentary
	information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	
Data aggregation methods	• *In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (e.g. cutting of high grades) and cut-off grades are usually Material and should be stated.* • *Where aggregate intercepts incorporate short lengths of high-grade results and longer lengths of low-grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.* • *The assumptions used for any reporting of metal equivalent values should be clearly stated.*	• Not applicable as exploration results are not reported.
Relationship between mineralisation widths and intercept lengths	• *These relationships are particularly important in the reporting of Exploration Results.* • *If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.* • *If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (e.g. 'down hole length, true width not known').*	• Not applicable as exploration results are not reported.
Diagrams	• *Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include but not be limited to a plan view of drill hole collar locations and appropriate sectional views.*	• Relevant plans, sections and supporting figures are included in the report.
Balanced reporting	• *Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.*	• Not applicable as exploration results are not reported.
Other substantive exploration data	• *Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.*	• Not applicable as exploration results are not reported.
Further work	• *The nature and scale of planned further work (e.g. tests for lateral extensions or depth extensions or large-scale step-out drilling).*	• Additional drilling is planned to occur at the PLS project including geophysical surveys, exploration drilling and resource-focused

Criteria	JORC Code explanation	Commentary
	• *Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.*	drilling.

Section 3 Estimation and Reporting of Mineral Resources

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary

Database integrity	• *Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes.*
	• *Data validation procedures used.*
		• The following digital checks were performed on the drillhole database as part of the Mineral Resource estimate, and no significant issues were identified:
		  ○ Header table: Searched for incorrect or duplicate collar coordinates and duplicate hole IDs.
		  ○ Survey table: Searched for duplicate entries, survey points beyond the maximum depth specified in the collar table, and abnormal dips and azimuths.
		  ○ Core recovery table: Searched for core recoveries greater than 100% or less than 80%, overlapping intervals, missing collar data, negative lengths, and data points beyond the maximum depth in the collar table.
		  ○ Lithology table: Searched for duplicate entries, intervals beyond the maximum depth in the collar table, overlapping intervals, negative lengths, missing collar data, missing intervals, and incorrect logging codes.
		  ○ Geochemical and assay table: Searched for duplicate entries, sample intervals beyond the maximum depth, negative lengths, overlapping intervals, sampling lengths exceeding tolerance levels, missing collar data, missing intervals, and duplicate sample IDs.

Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	• The project has been repeatedly visited by the Competent Person since 2012 with the most recent being for a three-week period in February – March 2026.
Geological interpretation	• *Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral*	• The geological setting of the Triple R deposit was considered well understood, having been the focus of extensive drill programs from 2012 through 2025, totalling

PALADIN

Criteria	JORC Code explanation	Commentary
	deposit. • *Nature of the data used and of any assumptions made.* • *The effect, if any, of alternative interpretations on Mineral Resource estimation.* • *The use of geology in guiding and controlling Mineral Resource estimation.* • *The factors affecting continuity both of grade and geology.*	542 drillholes with downhole orientation surveys and detailed geological and geotechnical logging. • The Triple R mineralization models largely followed the orientation of the regional basement geology, which dips steeply to the southeast, while also reflecting local-scale sub-horizontal structural controls that resulted from reverse kinematics along the primary fault zone hosting the uranium mineralization.
Dimensions	• *The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource.*	See table below
Estimation and modelling techniques	• *The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.* • *The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.* • *The assumptions made regarding recovery of by-products.* • *Estimation of deleterious elements or other non-*	• Wireframe models of mineralized zones were used to constrain block model uranium grade interpolations. Low-grade wireframe models were drafted using polylines snapped to mineralized intervals based on a cut-off grade of 0.05% U_3O_8 and a minimum core length of 1 m. The cut-off grade and minimum thickness were considered appropriate for Athabasca Basin uranium projects. High-grade domain wireframes used a cut-off grade of 5% U_3O_8, although lower grades were incorporated to maintain model continuity and meet the 1 m thickness requirement. • The Triple R deposit resource models comprised 80 sub-vertically stacked wireframes (domains) covering the R1515W, R840W, R00E, R780E, and R1620E mineralized zones. • Statistical and visual review of uranium assay data suggested capping high-grade values between 7–20% U_3O_8 in the low-grade domains, and between 35–55% U_3O_8 in the R840W and R780E high-grade domains. • Gold assays were capped at 15 g/t in the R780E high-grade domain and 10 g/t in all

Dimensions (Commentary):

Zone	Strike length (m)	Maximum Plan Width (m)	Top (masl)	Bottom (masl)
R1515W	104	143	450	258
R840W	433	60	447	174
R00E	121	46	447	408
R780E	956	109	453	156
R1620E	188	28	436	348

Criteria	JORC Code explanation	Commentary

	grade variables of economic significance (eg sulphur for acid mine drainage characterisation).
	• *In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.*
	• *Any assumptions behind modelling of selective mining units.*
	• *Any assumptions about correlation between variables.*
	• *Description of how the geological interpretation was used to control the resource estimates.*
	• *Discussion of basis for using or not using grade cutting or capping.*
	• *The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.*
		other wireframes. Gold is reported as a by-product Mineral Resource associated with the Triple R uranium mineralisation. No gold Ore Reserve is reported in this announcement.
		• Considering minimum mining width, uranium style, grade continuity, and sample length (99% being 0.5 m), a composite length of 2 m was chosen. Composites were created from the capped uranium assay values using boundaries defined by the wireframe domains.
		• Variograms were generated from the composite data, and continuity ranges were interpreted to be between 20–30 m.
		• The Mineral Resource was estimated using an Inverse Distance Cubed (ID3) method in a single pass, with a minimum of two and a maximum of seven U_3O_8 composites per block.
		• Search ellipse dimensions varied by domain, with most ellipses measuring 50 m × 50 m × 10 m.
		• To limit the influence of high-grade composites, grades exceeding designated threshold values for certain domains, determined using basic statistics and visual inspection, were restricted to a search ellipse of 25 m × 25 m × 5 m.
		• A block model was created using Vulcan software, with the lower-left corner located at UTM coordinates 596,304.821 mE, 6,388,726.026 mN, and 0.0 m elevation. The model comprised 737 columns, 380 rows, and 270 levels.
		• Block dimensions were 1 m wide, 2 m high, and 5 m along strike. The block model fully enclosed the resource domains and was oriented 66.2° to align with the overall mineralization orientation.
		• The block model was validated using multiple methods:
		  ○ Swath plots of composite grades versus interpolated ID3 and nearest neighbour grades
		  ○ Volumetric comparison of blocks versus wireframes
		  ○ Visual inspection of block versus composite grades on plan, vertical, and long sections
		  ○ Parallel secondary estimation using ID3
		  ○ Statistical comparison of block grades with assay and composite grades

Criteria	JORC Code explanation	Commentary
		• When comparing the May 17, 2022, Mineral Resource Estimate with the September 19, 2019, estimate, Indicated Mineral Resources increased by 21%, or approximately 472,000 t, with a slight decrease in grade from 2.10% U_3O_8 to 1.94% U_3O_8. Inferred Mineral Resources decreased by 48%, or approximately 586,000 t, with a grade reduction from 1.22% U_3O_8 to 1.10% U_3O_8. The Mineral Resource table in this announcement includes subsequent non-material updates to R840W and R1515W completed after the 17 May 2022 estimate.
Moisture	• *Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content.*	• All tonnages are estimated on a dry basis.
Cut-off parameters	• *The basis of the adopted cut-off grade(s) or quality parameters applied.*	• Using a US$50/lb uranium price, a cut-off grade of 0.25% U_3O_8 was determined to be appropriate for a potential underground mining scenario, based on comparisons with other Athabasca Basin uranium projects.
Mining factors or assumptions	• *Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made.*	• Due to the Triple R deposit depth below surface, mineralisation is expected to be extracted using conventional underground mining methods. • No mining dilution was applied to the Mineral Resource estimate. • Further information is provided in Section 4
Metallurgical factors or assumptions	• *The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where*	• A metallurgy and mineralogy scoping study of the Triple R deposit was carried out in 2013 to examine the metallurgical characteristics of the deposit, the relationships between ore and gangue, and the mineralogy, as well as how these characteristics varied spatially and across different rock types. • Five composite samples were produced from the R00E and R780E zones to represent the overall uranium mineralization. The uranium head grades of the composites ranged from 0.7% U_3O_8 to 3.4% U_3O_8, with an average grade of 1.78% U_3O_8. Uranium extraction ranged from 95% to 99.4%, averaging 98.1%, when

Criteria	JORC Code explanation	Commentary

	this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.	leached at a grind size of P85 = 250 µm, temperatures of 45–55°C, free acid levels of 25 g/L, a final oxidation-reduction potential of 450 mV, and a leach retention time of six hours.
		• One master composite sample was prepared using the five sub-composite samples. The master composite had a head grade of 2.09% U_3O_8. Uranium extraction of 98.4% was achieved in six hours at 50°C and atmospheric pressure with 54 kg of acid added per tonne of leach feed. Leach efficiency was similar across grind sizes (P85) from 75 µm to 250 µm, indicating that uranium minerals could be liberated at relatively coarse grind sizes.
		• In 2017 a Pre-Feasibility metallurgical program was led by Melis Engineering Ltd. and conducted at the SGS laboratory in Lakefield, Ontario, testing multiple mineralized composites representing different host rock lithologies and uranium grades. Three HQ-sized drillholes were completed at R780E to provide enough material for composite sample creation. In total, twenty-six sub-composite samples were assembled consisting of 12 composites spatially representing different host rock lithologies and a range of uranium grades from 0.51 – 25.9% U_3O_8, two composites from shallow and deep mineralization, three composites in line with the conceptual mine schedule uranium grades for years 1, 2 and 6, one low-grade composite near the cut-off grade, four comminution composites and four gangue composites.
		• The following results were obtained:
		  ○ Comminution testing: Three host rock lithology blends and one gangue composite were tested for grindability. The results showed the material ranged from very soft to soft for SAG milling and soft to moderately soft for ball milling, indicating relatively easy crushing/grinding characteristics.
		  ○ Leach testing: Leach tests were completed on 22 composite mineralized samples. Optimal conditions were identified, including a grind size of P80 ≈150 µm, 45–50% solids, eight hours leach time at ~50 °C, and controlled acid and oxidant conditions. Under these conditions, uranium extraction ranged from about 94.6% to 98.8%. Projected net recoveries were approximately 97.1% for higher-grade material and 94.9% for lower-grade material.

Criteria	JORC Code explanation	Commentary
		○ Liquid/solid separation thickening and rheology tests were completed on leach residue from the bulk leach test on the composites. Counter Current Decantation (CCD) simulations using the test data showed that a pregnant leach solution to ore ratio of 3.0:1 and a total of six thickeners would provide a target soluble loss of ≤ 0.5% in the CCD circuit. ○ SX batch and mini continuous tests on PLS pregnant leach solutions showed that strong acid stripping was more efficient (99.6%) than ammonium sulfate (95%). The results supported a flowsheet with four-stage extraction, two-stage scrub, five-stage strong acid strip, and single-stage acid recovery and regeneration. ○ Gypsum precipitation prevented excess sulfate contamination, followed by uranium peroxide precipitation. The strong acid strip circuit produced higher-quality yellowcake (81.2% U_3O_8) with overall uranium recoveries of 97.1% for 2% feed grade and 94.9% for 0.5% feed grade.
Environmental factors or assumptions	• *Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.*	• This information is provided as part of Section 4.
Bulk density	• *Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and*	• Samples for bulk density analysis were collected every 2.5 m through the mineralized zones at Triple R. Bulk density samples consisted of an approximately 5 cm long piece of full NQ-sized core.

Criteria	JORC Code explanation	Commentary
	representativeness of the samples. • *The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.* • *Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.*	• Bulk density samples were analysed using the Density 3 Package at the SRC Geoanalytical Laboratory in Saskatoon, Saskatchewan. Samples were dried and weighed, then coated with an impermeable layer of wax and re-weighed. The samples were then weighed while submerged in water. All weights were entered into a database, and the rock density was calculated for each sample. The temperature of the water was recorded during all measurements and included in the calculations. The detection limit for Density 3 analysis was 0.01 g/cc. • Block uranium grade values and density values were estimated independently. Block densities were estimated from the density measurements using inverse distance cubed (ID3) with a search strategy similar to that used for uranium grade. Hard boundaries were applied between resource domains. The Triple R resource database included 17,509 density measurements, of which 15,920 were used in the resource estimation.
Classification	• *The basis for the classification of the Mineral Resources into varying confidence categories.* • *Whether appropriate account has been taken of all relevant factors (i.e. relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).* • *Whether the result appropriately reflects the Competent Person's view of the deposit.*	• Mineral Resources were classified as Indicated or Inferred based on drillhole spacing and the apparent continuity of mineralization. ▪ Indicated Mineral Resources are defined as blocks within the domains where drill sections are spaced 15 m apart along strike, vertical holes are spaced approximately 10 m to 15 m along each section, grade continuity indicated by two or more drill holes that meet the minimum cut-off criteria (0.05% U_3O_8), and a distance to nearest neighbour less than 15 m. Angle holes are spaced from 15 m to 45 m apart, averaging 30 m, along the strike direction. ▪ Inferred Mineral Resources are defined as all remaining blocks within the domains that are not classified as Indicated.
Audits or reviews	• *The results of any audits or reviews of Mineral Resource estimates.*	• No audits or reviews of the Mineral Resource estimate took place.
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application*	• The following factors were considered when classifying the Mineral Resources: ○ Drilling, sampling, sample preparation, and assay procedures were determined to follow industry standards. ○ Data verification and validation work confirmed drill hole sample databases

Criteria	JORC Code explanation	Commentary
	of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate. • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	are reliable. ○ No significant biases were observed in the QA/QC analysis results. ○ Confidence in interpretation and modelling of geological and estimation domains. ○ Mineralization domains are interpreted manually in cross-sections and refined in longitudinal sections by an experienced resource geologist. ○ There is good agreement between the drill holes and mineralization wireframe shapes. ○ Indicated block grades correlate well with composite data, statistically and spatially, and locally and globally.

Section 4 Estimation and Reporting of Ore Reserves

(Criteria listed in section 1, and where relevant in sections 2 and 3, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral Resource estimate for conversion to Ore Reserves	• *Description of the Mineral Resource estimate used as a basis for the conversion to an Ore Reserve.* • *Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Ore Reserves.*	• The Mineral Resource estimate used as the basis for conversion to Ore Reserves was the Triple R Mineral Resource estimate with an effective date of 17 May 2022. The Mineral Resource estimate reported in this announcement includes subsequent non-material Mineral Resource updates for the R840W and R1515W zones; these later updates were not used to derive the reported Ore Reserve. • Mineral Resources are inclusive of the Ore Reserves.
Site visits	• *Comment on any site visits undertaken by the Competent Person and the outcome of those visits.* • *If no site visits have been undertaken indicate why this is the case.*	• The property was visited by the Maurice Mostert, a former employee of Mining Plus, on October 13 and 14, 2021. • Lewis Kitchen has not visited the property.
Study status	• *The type and level of study undertaken to enable Mineral Resources to be converted to Ore Reserves.* • *The Code requires that a study to at least Pre-*	• A Feasibility-level study was completed for the Triple R deposit and PLS property with an effective date of 17 January 2023.

Criteria	JORC Code explanation	Commentary
	Feasibility Study level has been undertaken to convert Mineral Resources to Ore Reserves. Such studies will have been carried out and will have determined a mine plan that is technically achievable and economically viable, and that material Modifying Factors have been considered.	
Cut-off parameters	• *The basis of the cut-off grade(s) or quality parameters applied.*	• Ore Reserves are reported above an underground cut-off grade of 0.25% U_3O_8. The cut-off grade is supported by the Feasibility Study economic assumptions, including a long-term uranium price of US$65/lb U_3O_8, operating cost estimates, metallurgical recovery assumptions, and applicable Saskatchewan revenue and royalty assumptions.

Mining factors or assumptions	• *The method and assumptions used as reported in the Pre-Feasibility or Feasibility Study to convert the Mineral Resource to an Ore Reserve (i.e. either by application of appropriate factors by optimisation or by preliminary or detailed design).*
	• *The choice, nature and appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc.*
	• *The assumptions made regarding geotechnical parameters (eg pit slopes, stope sizes, etc), grade control and pre-production drilling.*
	• *The major assumptions made and Mineral Resource model used for pit and stope optimisation (if appropriate).*
	• *The mining dilution factors used.*
	• *The mining recovery factors used.*
	• *Any minimum mining widths used.*
	• *The manner in which Inferred Mineral Resources are utilised in mining studies and the sensitivity of the outcome to their inclusion.*
	• *The infrastructure requirements of the selected mining methods.*
		• Initial MSO stope optimisation used a 0.2% U_3O_8 cut-off to generate candidate mining shapes. The MSO outputs were evaluated in the context of mine design, geotechnical constraints, dilution, mining recovery and scheduling assumptions, with the final Ore Reserve reported above the 0.25% U_3O_8 reporting cut-off. For longhole stoping, a minimum mining width of 4 m (including hanging wall and footwall dilution) and stope height of 20 m was used. Following MSO, the mineable shapes were further subdivided in Deswik to produce a maximum width of 12 m (including hanging wall and footwall dilution). Drift and fill mining is designed at 5 m wide by 5 m high for development shapes located in the crown pillar areas of the orebodies.
		• Mining recovery of 95% was applied to all stopes, while all development mining assumes 100% extraction.
		• Mineral Resource to Reserve conversion for Indicated material was 84.2% within the R840W, R00E, and R780E zones. Mining losses fall primarily within the following two categories:
		  ○ Sterilization of material located within the designed crown pillar.
		  ○ Resource blocks being excluded from designed stopes due to low grades or inadequate continuity with adjacent mineralization.
		• The primary mining method envisioned for the PLS project is longhole sublevel retreat stoping in the longitudinal direction. Stopes were generated using Datamine MSO software with the following parameters:
		  ○ Stope Height (floor to floor direction): 20 m

Criteria	JORC Code explanation	Commentary
		○ Stope Length (longitudinal along strike): 10 m ○ Minimum Stope Width: 4 m ○ Maximum Stope Width: 12 m ○ Minimum Stope Dip: 75° ○ Optimization Orientation -23.8° ○ Initial Cut Off Grade: 0.2 % U_3O_8 • Due to geotechnical constraints and proximity to the bedrock contact, the crown pillar zones above 420 m elevation of the deposits are planned to be mined via drift and fill. These are currently designed as 5 m wide by 5 m high development drifts utilizing cemented hydraulic backfill to extract multiple passes where the orebody thickness exceeds 5 m. Drift and fill shapes were generated using Datamine MSO software using the spatial parameters below. ○ Drift Height: 5 m ○ Drift Width: 5 m ○ Pillar: 0 m ○ Dip: 90° ○ Maximum Waste: 30% ○ Initial Cut-Off Grade: 0.2% • Any inferred material within a reserve stope shape has also been assigned a grade of 0% during the Ore Reserve calculation. • A hybrid approach to applying dilution to longhole stoping has been used for the PLS project. While a minimum longhole mining width of 2 m is practically achievable, the MSO minimum mining width parameter was forced to 4 m to account for 2 m of combined hanging wall and footwall overbreak. A 10 m maximum mining width has also been assumed, but when accounting for 2 m of overbreak, a realistic parameter of 12 m has been used. Further dilution was then added during the scheduling phase to account for backfill dilution and spatial constraints. The dilution applied within the schedule is assumed to be at zero grade, whereas when dilution has been applied through MSO, the grade is based on block model values. • There are two parameters being used to determine the additional external dilution: ○ Backfill wall exposure: Stopes have been manually assigned whether

Criteria	JORC Code explanation	Commentary
		they will have end wall or sidewall backfill exposure to account for differences in backfill dilution. Sidewall exposure occurs in areas of the orebody where widths are more than 12 m, and multiple stopes must be mined in the transverse direction to fully extract the ore. In effect, this means once the initial or primary stope is mined, all subsequent or secondary stopes in sequence will have side walls consisting of cemented fill. ○ Proximity to hanging wall and footwall contacts: In areas where stopes are mined within 5 m to 7 m of the Mineralized Shear Zone (MSZ) contact, it is expected that additional dilution will occur, as stopes will naturally want to break to the geological unit contacts. The risk is expected to be partially mitigated using cable bolting where required. Development, including drift-and-fill mining, has been assigned an overbreak/dilution factor of 5%, which has a 0% grade assigned to the waste dilution. • An analysis of the planned underground stope shapes has been performed and shows a net dilution of 24%. • For the PLS project, a longhole mining recovery of 95% has been applied, while development mining assumes 100%.
Metallurgical factors or assumptions	• *The metallurgical process proposed and the appropriateness of that process to the style of mineralisation.* • *Whether the metallurgical process is well-tested technology or novel in nature.* • *The nature, amount and representativeness of metallurgical test work undertaken, the nature of the metallurgical domaining applied and the corresponding metallurgical recovery factors applied.* • *Any assumptions or allowances made for deleterious elements.* • *The existence of any bulk sample or pilot scale test*	• Four HQ-sized drillholes were completed in 2021 at the R840W zone to provide additional uranium mineralization for metallurgical characterization. The four metallurgical drillholes covered the east and west parts of R840W, at upper, middle and lower elevation ranges relative to the deposit. • Existing metallurgical material from the 2017 R780E test work was blended with the 2021 R840W material at a 75%/25% ratio, respectively. • Bench-scale and bulk metallurgical tests were performed at SGS Lakefield to support Feasibility level plant design and demonstrated strong performance across all conditions tested. The following results were determined: ○ Leaching: 98.4% average uranium extraction in 12 hours. ○ CCD circuit: Six-stage design achieved 99.5% wash efficiency. ○ Solvent extraction: 99.9% uranium recovery and 99.4% stripping

Criteria	JORC Code explanation	Commentary
	work and the degree to which such samples are considered representative of the orebody as a whole. • *For minerals that are defined by a specification, has the ore reserve estimation been based on the appropriate mineralogy to meet the specifications?*	efficiency in mini-pilot testing. ○ Gypsum precipitation: >95% uranium re-dissolution, reducing cake grade to ~0.025% U_3O_8. ○ Yellowcake production: 80% U_3O_8 precipitate; 95% U_3O_8 after calcining at 450°C. • Overall, test work confirmed high uranium recovery and production of refinery-grade yellowcake. • Carbon-in-leach tests were carried out on the washed acid leach residue from the bulk leach with varying leach retention times. The total gold extraction increased to 91.7% with a 48-hour leach, with 86.6% of the gold recovered on carbon. The total silver extraction achieved for a 48-hour leach was 76.5%, with 74.3% recovered on carbon for a 2.12 g/t Ag head grade. The gold recovery on carbon, 86.6% for a 48-hour leach based on a calculated head grade of 0.30 g Au/t, was higher than the previously achieved 79.3% recovery on Composite in the Pre-Feasibility test work, with a similar calculated head grade of 0.34 g Au/t. Gold metallurgical test work is disclosed for completeness; however, no gold Ore Reserve is reported in this announcement.
Environmental	• *The status of studies of potential environmental impacts of the mining and processing operation. Details of waste rock characterisation and the consideration of potential sites, status of design options considered and, where applicable, the status of approvals for process residue storage and waste dumps should be reported.*	• The Environmental Impact Statement (EIS) for the PLS project was submitted to the Saskatchewan Ministry of Environment in June 2025, summarizing over a decade of baseline environmental data and assessing interactions between the project and the environment, including mitigation measures. Paladin received Ministerial approval for the EIS under Saskatchewan's Environmental Assessment Act in February 2026. • The EIS process included baseline field programs and consultation with local Indigenous Nations and stakeholders. • The EIS reported that “potential environmental impacts of the Project would be minimal and manageable” and that appropriate controls and mitigation measures had been developed for identified risks. • Baseline work included hydrogeological and geotechnical investigations to support the siting of facilities such as the tailings management facility (TMF), waste rock stockpiles, surface infrastructure, and drainage planning.

Criteria	JORC Code explanation	Commentary
		• Waste rock, beneficiation reject, and tailings characterization programs were conducted as part of earlier environmental scoping work. • The Feasibility Study and related design work included preliminary TMF design and evaluation of candidate sites to minimize environmental risk, considering water quality and hydrogeological factors. • The TMF and water handling systems were designed so that excess water could be returned to the process plant for treatment and controlled release, and the TMF could also act as interim water storage during high precipitation events. • The Feasibility Study and concurrent pre-environmental planning work identified optimal locations for the processing plant, TMF, and other surface infrastructure to reduce environmental footprint and limit interactions with sensitive features such as Patterson Lake and local biodiversity. • Infrastructure was arranged to maintain buffers to aquatic features and avoid old-growth forests and heritage sites wherever feasible.
Infrastructure	• *The existence of appropriate infrastructure: availability of land for plant development, power, water, transportation (particularly for bulk commodities), labour, accommodation; or the ease with which the infrastructure can be provided, or accessed.*	• The PLS project had year-round access via Highway 955 and covered about 31,039 ha, providing sufficient space for mine development and infrastructure. • The site infrastructure is planned to include an underground mine, process plant, waste rock management facility, tailings management facility, camp, and internal roads. • Power was planned to be supplied by an on-site light natural gas power plant, while water would come mainly from groundwater wells and Patterson Lake, with additional sources such as mine dewatering and reclaimed water. • Supporting infrastructure included a communications tower, mine facilities (ventilation shafts, access decline, freeze plant, dewatering wells, and backfill plant), and tailings systems with water treatment ponds for safe water and tailings management.
Costs	• *The derivation of, or assumptions made, regarding projected capital costs in the study.* • *The methodology used to estimate operating costs.* • *Allowances made for the content of deleterious*	• An initial capital cost of C$1.155 billion was estimated for the Feasibility Study. • Vendor quotations were obtained for major equipment including vendor-provided prices, delivery lead times, spare allowances, and freight costs to project location. The quotations used in the Feasibility Study cost estimate were obtained in Q3/Q4

Criteria	JORC Code explanation	Commentary
	elements. • *The source of exchange rates used in the study.* • *Derivation of transportation charges.* • *The basis for forecasting or source of treatment and refining charges, penalties for failure to meet specification, etc.* • *The allowances made for royalties payable, both Government and private.*	2022. • For non-major equipment, costing was based on in-house data or quotes from other projects in the region. All equipment and material costs include Incoterms Free Carrier. Other costs such as spares, taxes, duties, freight, and packaging are covered separately in the cost estimate as indirect costs. • The PLS project operating cost estimate consists of mining, processing, and general and administration costs. The average operating cost is estimated at C$393/t ore processed, or C$13.02/lb U_3O_8 produced. • All currencies are expressed in Canadian dollars, unless otherwise stated. Where required, costs have been converted using fixed currency exchange rates of US$0.75/EUR€0.72/AUD$1.09 to C$1.00. • The PLS project does not have private royalties; the primary royalty burden is the Saskatchewan uranium crown royalty regime. This was factored into the PLS project revenue.
Revenue factors	• *The derivation of, or assumptions made regarding revenue factors including head grade, metal or commodity price(s) exchange rates, transportation and treatment charges, penalties, net smelter returns, etc.* • *The derivation of assumptions made of metal or commodity price(s), for the principal metals, minerals and co-products.*	• Metal revenues were calculated based on the metal recoveries and life-of-mine U_3O_8 production schedule and the metal pricing determined by uranium market analysis. Operating cost for mining, processing, site services, general and administration, tailings management and handling and effluent treatment, as well as off-site charges (smelting, refining, transportation, and royalties) were deducted from the revenues to derive annual operating cash flow.
Market assessment	• *The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future.* • *A customer and competitor analysis along with the identification of likely market windows for the product.* • *Price and volume forecasts and the basis for these forecasts.*	• Market demand for yellowcake uranium was based on the International Energy Agency 2021 World Energy Outlook which expects a 75% increase in energy requirements by 2050 with an estimated 56 new nuclear reactors currently under construction. These assumptions formed part of the Feasibility Study basis for the Ore Reserve. • Market supply of yellowcake was assessed relative to expected market demand with a supply gap identified beginning in the late-2020s. • Using the UxC LLC Uranium Market Outlook Q3 2022 data a modest forecasted

Criteria	JORC Code explanation	Commentary
	• *For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.*	U_3O_8 price of US$65/lb was assumed for the PLS project.

Economic	• *The inputs to the economic analysis to produce the net present value (NPV) in the study, the source and confidence of these economic inputs including estimated inflation, discount rate, etc.*
	• *NPV ranges and sensitivity to variations in the significant assumptions and inputs.*
		• Economic analysis of the Feasibility Study demonstrates that the PLS project is economically viable using the price assumptions, cost estimates and technical parameters generated by the Feasibility Study. Using an annual discount rate of 8%, the project base case post-tax cash flow evaluates to a net present value (NPV) of C$1.204 billion and an internal rate (IRR) of return of 27.2%. The post-tax payback period is 2.6 years when discounted at 8% per year based on the metal price of US$65/lb U_3O_8 and the exchange rate of C$1.00 to US$0.75.
		• The sensitivity of NPV, IRR, and payback period were investigated relative to the following key variables. Each of key variables was changed between -30% and +30% in 10% increments while holding the other variables constant, except for metal recovery in %, which was changed in 0.5 increments. Sensitivity analyses were carried out on the following key variables:
		  ○ Uranium metal price (U_3O_8)
		  ○ Head Grade
		  ○ Exchange rate
		  ○ Capital costs
		  ○ Operating costs
		  ○ Metal process recovery
		• The NPV is most sensitive to exchange rate, uranium price and head grade, followed by capital costs, operating costs, and metal recovery. The IRR is most sensitive to capital costs, exchange rate, uranium price and head grade, followed by operating costs, and metal recovery.

Social	• *The status of agreements with key stakeholders and matters leading to social licence to operate.*	• The PLS Environmental Impact Study has been approved by the Saskatchewan provincial authorities. Community engagement activities are ongoing as part of permitting, which aligns with early elements of achieving societal acceptance and regulatory compliance. This includes baseline studies, reporting and data compilation with engagement activities documented as part of the environmental assessment process. No material social or stakeholder matters have been identified

Criteria	JORC Code explanation	Commentary
		that are expected to prevent development of the Ore Reserve, subject to the receipt of remaining permits and approvals. The existence of the Metis challenge does not of itself prevent extraction of the ore reserve.
Other	• *To the extent relevant, the impact of the following on the project and/or on the estimation and classification of the Ore Reserves:* • *Any identified material naturally occurring risks.* • *The status of material legal agreements and marketing arrangements.* • *The status of governmental agreements and approvals critical to the viability of the project, such as mineral tenement status, and government and statutory approvals. There must be reasonable grounds to expect that all necessary Government approvals will be received within the timeframes anticipated in the Pre-Feasibility or Feasibility study. Highlight and discuss the materiality of any unresolved matter that is dependent on a third party on which extraction of the reserve is contingent.*	• Mineral claims comprising the PLS project remain secure. • The province of Saskatchewan has an extensive history of uranium mining operations and an established regulatory framework for uranium development. • Paladin Canada Inc. is working with provincial and Federal regulators to gain necessary approvals to advance the PLS project towards becoming an active mine. • Based on the current status of environmental assessment approval, tenure security and ongoing permitting activities, there are reasonable grounds to expect that the remaining approvals required for development can be obtained within the timeframes contemplated by the Feasibility Study. No material unresolved third-party matters have been identified that would prevent extraction of the Ore Reserve.
Classification	• *The basis for the classification of the Ore Reserves into varying confidence categories.* • *Whether the result appropriately reflects the Competent Person's view of the deposit.* • *The proportion of Probable Ore Reserves that have been derived from Measured Mineral Resources (if any).*	• Ore Reserve classification at PLS is based on the confidence in the underlying Mineral Resource, the level of study completed, and the consideration of the Modifying Factors. In accordance with the JORC Code (2012), Ore Reserves have been classified as Probable Ore Reserves. No Proven Ore Reserves are reported. No Inferred Mineral Resources have been included in the Ore Reserve estimate. • The Ore Reserve estimate includes material converted from Indicated Mineral Resources to Probable Ore Reserves where the modifying factors and mine design support that level of confidence. • Mineral Resource to Ore Reserve conversion for Indicated material was 84.2% within the R840W, R00E, and R780E zones.
Audits or reviews	• *The results of any audits or reviews of Ore Reserve estimates.*	• There has been no external audit of the Ore Reserve. • The Mineral Reserve and supporting modifying factors were reviewed by the Competent Person for reporting under the JORC Code (2012), and no material issues were identified.

Criteria	JORC Code explanation	Commentary
Discussion of relative accuracy/ confidence	• *Where appropriate a statement of the relative accuracy and confidence level in the Ore Reserve estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the reserve within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors which could affect the relative accuracy and confidence of the estimate.* • *The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.* • *Accuracy and confidence discussions should extend to specific discussions of any applied Modifying Factors that may have a material impact on Ore Reserve viability, or for which there are remaining areas of uncertainty at the current study stage.* • *It is recognised that this may not be possible or appropriate in all circumstances. These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.*	• The confidence in the Ore Reserve estimate is derived from the confidence in the underlying Mineral Resource estimate and the level of confidence in the modifying factors applied through the Feasibility Study as outlined in Section 3.

Appendix 1: Drillhole Collars

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS12-004	597844.0	6389813.0	499.7	142.3	0	-90
PLS12-013	597061.0	6389469.0	546.5	192.0	0	-90
PLS12-014	597047.0	6389481.0	546.5	185.0	0	-90
PLS12-015	597141.0	6389595.0	545.0	189.3	0	-90
PLS12-016	597799.0	6389835.0	505.0	224.6	0	-90
PLS12-018	596989.6	6389393.9	547.8	178.9	0	-90
PLS12-019	597064.3	6389461.4	547.1	203.3	0	-90
PLS12-022	597794.0	6389842.8	505.4	212.5	0	-90
PLS12-023	597789.4	6389852.7	506.0	197.2	0	-90
PLS12-024	597784.0	6389845.2	506.1	192.0	0	-90
PLS12-025	597778.3	6389853.0	507.3	161.6	0	-90
PLS13-026	597765.6	6389845.5	509.2	172.8	320	-86
PLS13-027	597770.3	6389835.3	509.0	255.1	346	-89
PLS13-028	597876.2	6389880.1	499.0	203.3	47	-90
PLS13-029	597762.7	6389852.9	509.4	203.3	349	-89
PLS13-030	597872.2	6389888.0	499.0	183.0	46	-90
PLS13-031	597757.1	6389861.1	510.5	194.2	356	-89
PLS13-032	597879.6	6389870.8	499.0	197.2	23	-90
PLS13-033	597752.4	6389870.0	511.0	172.8	177	-90
PLS13-034	597890.3	6389884.1	499.0	188.1	339	-90
PLS13-035	597796.6	6389816.1	506.9	215.5	337	-71
PLS13-036	597894.9	6389874.7	499.0	188.1	176	-89
PLS13-037	597773.9	6389828.2	508.6	276.5	45	-88
PLS13-038	598159.9	6389973.4	499.0	221.6	11	-90
PLS13-039	597755.0	6389830.0	509.6	282.6	99	-89
PLS13-041	597747.5	6389849.3	511.0	197.2	100	-89
PLS13-043	597751.4	6389839.9	510.7	197.2	251	-89
PLS13-044	598156.8	6389982.5	499.0	197.2	268	-90
PLS13-045	597741.2	6389859.4	511.0	182.0	357	-89
PLS13-046	598166.1	6389965.9	499.0	307.0	277	-89
PLS13-047	597731.5	6389833.7	512.0	246.0	44	-89
PLS13-048	598522.5	6390125.1	499.0	215.5	11	-88
PLS13-049	597728.3	6389843.0	509.8	209.4	76	-89
PLS13-050	597724.4	6389852.3	510.5	233.8	266	-88
PLS13-051	598175.7	6389981.1	499.0	282.6	256	-90
PLS13-052	597798.1	6389834.6	506.5	194.2	23	-69
PLS13-053	598145.9	6389969.7	499.0	282.6	66	-89
PLS13-054	597805.7	6389826.1	508.0	200.3	15	-71
PLS13-055	598527.3	6390110.3	499.0	261.2	115	-89
PLS13-056	597792.5	6389840.8	506.6	197.2	23	-71

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS13-058	597778.3	6389861.1	506.9	194.2	262	-89
PLS13-059	597834.9	6389847.6	499.0	194.2	301	-72
PLS13-060	598532.3	6390101.1	499.0	276.5	0	-90
PLS13-061	598134.5	6389964.7	499.0	291.7	91	-89
PLS13-062	598144.0	6389978.3	499.0	212.5	57	-89
PLS13-064	598171.9	6389988.7	499.0	218.5	202	-89
PLS13-065	597847.8	6389865.8	499.0	218.5	256	-90
PLS13-066	598190.4	6389986.5	499.0	279.5	234	-89
PLS13-067	597837.4	6389855.5	499.0	209.4	24	-89
PLS13-068	598153.9	6389991.7	499.0	236.8	21	-90
PLS13-069	597834.7	6389864.7	499.0	185.0	17	-89
PLS13-070	598150.1	6390000.1	499.0	258.2	123	-90
PLS13-071	597827.0	6389871.8	499.0	108.8	0	-90
PLS13-072	598119.7	6389960.0	499.9	209.0	351	-89
PLS13-073	598205.9	6389993.4	499.7	248.0	132	-89
PLS13-074	597715.0	6389836.9	512.3	203.0	76	-89
PLS13-075	598106.5	6389952.7	499.7	248.0	164	-89
PLS13-076	597777.0	6389818.0	505.3	267.0	60	-89
PLS13-077	597788.3	6389853.4	506.2	259.5	338	-84
PLS13-078	598202.1	6389999.1	499.6	224.0	315	-89
PLS13-079	597805.8	6389826.0	504.4	218.0	26	-75
PLS13-080	598534.6	6390091.3	499.7	347.0	344	-89
PLS13-081	598169.5	6389997.4	499.6	230.0	315	-90
PLS13-082	598545.1	6390117.0	499.7	380.0	141	-89
PLS13-083	598091.1	6389949.2	499.7	278.0	349	-89
PLS13-084	598676.5	6390181.5	499.7	350.0	160	-89
PLS13-085	598101.9	6389964.3	499.6	224.0	339	-89
PLS13-086	598136.3	6389956.5	499.6	263.0	266	-89
PLS13-087A	598089.2	6389957.6	499.6	227.0	153	-88
PLS13-088	598244.3	6390007.7	499.6	296.0	330	-89
PLS13-089	598524.2	6390086.2	499.7	393.0	22	-89
PLS13-090	598860.7	6390282.2	499.6	323.0	133	-89
PLS13-091	598030.5	6389877.5	499.6	373.0	139	-90
PLS13-092	598673.1	6390190.7	499.6	377.0	184	-89
PLS13-093	598012.7	6389906.3	499.6	278.0	346	-89
PLS13-094	598217.8	6389996.9	499.6	272.3	245	-90
PLS13-095	598078.4	6389941.6	499.6	275.0	60	-90
PLS13-096	598664.1	6390176.4	499.5	365.0	267	-89
PLS13-097	598550.8	6390098.2	499.6	356.0	301	-90
PLS13-098	598351.1	6390044.9	499.6	317.0	93	-89
PLS13-099	598692.0	6390185.8	499.6	368.0	223	-89
PLS13-100	598214.2	6390005.6	499.5	263.0	285	-89

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS13-101	598563.2	6390106.2	499.5	350.0	290	-90
PLS13-102	598081.7	6389932.8	499.6	275.0	333	-89
PLS13-103	598867.0	6390273.8	499.6	427.0	96	-89
PLS13-104	598231.7	6390003.0	499.6	309.2	84	-90
PLS13-105	598526.4	6390087.4	499.5	419.0	136	-90
PLS13-106	598345.6	6390053.4	499.5	332.0	85	-90
PLS13-107	598519.3	6390095.0	499.6	402.0	233	-89
PLS13-108	598560.2	6390114.3	499.5	392.0	40	-90
PLS13-109	598505.7	6390089.1	499.6	401.0	303	-90
PLS13-112	597049.6	6389481.0	547.3	248.0	321	-74
PLS13-114	597140.5	6389595.6	544.0	206.0	334	-73
PLS13-116	597223.2	6389648.1	540.5	323.0	333	-73
PLS13-118	597223.8	6389646.7	538.9	314.0	328	-89
PLS13-121	597219.9	6389656.9	540.4	248.0	211	-90
PLS13-122	597238.2	6389653.9	541.6	332.0	138	-89
PLS13-123	597234.2	6389663.1	541.7	260.0	106	-89
PLS13-124	597206.6	6389650.3	540.8	257.0	40	-88
PLS14-125	598331.8	6390033.0	499.0	359.0	200	-90
PLS14-126	598545.2	6390072.2	499.0	443.0	337	-90
PLS14-127	598573.2	6390118.7	499.0	350.0	91	-90
PLS14-128	598684.8	6390164.1	499.0	464.0	124	-90
PLS14-129	598360.7	6390043.1	499.0	344.0	239	-90
PLS14-130	598121.2	6389951.4	499.0	317.0	290	-90
PLS14-131	598549.0	6390063.0	499.0	494.0	199	-87
PLS14-132	598565.9	6390099.5	499.0	437.0	340	-90
PLS14-133	598095.5	6389940.3	499.0	401.0	51	-90
PLS14-134	598233.9	6389994.9	499.0	320.0	284	-90
PLS14-135	598695.8	6390175.9	499.0	386.0	348	-90
PLS14-136	598365.1	6390035.5	499.0	317.0	176	-87
PLS14-137	598170.3	6389956.5	499.0	335.0	186	-87
PLS14-138	598064.0	6389935.9	499.0	305.0	59	-90
PLS14-139	598353.8	6390034.3	499.0	425.0	164	-90
PLS14-140	598556.1	6390047.8	499.0	527.0	285	-90
PLS14-141	598705.5	6390192.1	499.0	351.8	114	-90
PLS14-142	598249.1	6389997.7	499.0	353.0	136	-90
PLS14-143	598337.1	6390024.6	499.0	368.0	178	-90
PLS14-144	598509.5	6390081.3	499.0	404.0	199	-90
PLS14-145	598578.1	6390109.8	499.0	422.0	241	-90
PLS14-146	598654.5	6390159.1	499.0	416.0	275	-90
PLS14-147	598376.6	6390045.3	499.0	359.0	248	-90
PLS14-148	598514.9	6390104.2	499.0	296.0	337	-90
PLS14-149	598179.2	6389972.7	499.0	319.1	60	-90

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS14-150	598657.9	6390151.1	499.0	374.0	309	-90
PLS14-151	598371.4	6390055.5	499.0	332.0	23	-90
PLS14-153	598614.9	6390136.3	499.0	382.0	1	-90
PLS14-155	598559.9	6390038.1	499.0	542.0	62	-90
PLS14-156	598477.8	6390075.0	499.0	377.0	189	-90
PLS14-157	598068.6	6389926.7	499.0	308.0	104	-90
PLS14-158	598723.4	6390188.9	499.0	374.0	337	-90
PLS14-159	598114.1	6389970.1	499.0	275.0	67	-90
PLS14-160	598305.1	6390023.4	499.0	356.0	115	-90
PLS14-161	598671.0	6390158.1	499.0	353.0	307	-90
PLS14-163	597834.4	6389831.7	499.0	275.0	327	-79
PLS14-164	598570.0	6390090.1	499.0	452.0	68	-90
PLS14-165	598307.7	6390015.0	499.0	362.0	115	-90
PLS14-166	598700.2	6390166.8	499.0	374.0	13	-90
PLS14-167	598130.5	6389973.1	499.0	308.0	221	-90
PLS14-169	598059.7	6389945.7	499.0	327.5	238	-90
PLS14-170	598650.2	6390168.1	499.0	347.0	0	-90
PLS14-171	598448.8	6390065.4	499.0	329.0	0	-90
PLS14-172	598582.2	6390099.9	499.0	332.0	78	-90
PLS14-173	598035.4	6389927.8	499.0	257.0	135	-90
PLS14-174	598445.9	6390073.9	499.0	290.0	10	-90
PLS14-175	598619.0	6390127.1	499.0	407.0	249	-90
PLS14-176	599165.4	6390443.8	499.0	359.0	349	-90
PLS14-177	598297.0	6390000.5	499.0	335.0	334	-80
PLS14-178	598512.8	6390071.8	499.0	500.0	210	-90
PLS14-179	598592.1	6390114.0	499.0	372.4	1	-90
PLS14-180	598719.2	6390198.2	499.0	344.0	90	-90
PLS14-181	598332.0	6390011.4	499.0	317.0	332	-84
PLS14-183	598588.2	6390122.8	499.0	341.0	27	-90
PLS14-184	598328.5	6390043.0	499.0	332.0	116	-90
PLS14-185	598742.5	6390181.3	499.0	347.8	329	-83
PLS14-186	598527.7	6390076.2	499.0	401.0	355	-90
PLS14-187	598421.3	6390055.2	499.0	441.8	220	-90
PLS14-189	598811.4	6390207.0	499.0	500.0	192	-90
PLS14-190	598874.6	6390259.9	499.0	431.6	10	-90
PLS14-191	598482.3	6390062.5	499.0	316.0	338	-82
PLS14-192	598400.3	6390028.5	499.0	320.0	332	-82
PLS14-193	598488.3	6390089.2	499.0	302.0	331	-90
PLS14-194	598746.3	6390172.7	499.0	386.0	336	-83
PLS14-195	598641.6	6390111.0	499.0	419.0	334	-83
PLS14-196	599286.9	6390467.9	499.0	392.0	291	-90
PLS14-197	598439.1	6390050.7	499.0	284.0	333	-83

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS14-198	598463.9	6390070.2	499.0	398.0	17	-90
PLS14-199	598811.2	6390195.4	499.0	485.7	333	-84
PLS14-200	598436.1	6390060.2	499.0	389.0	268	-90
PLS14-201	598613.4	6390100.4	499.0	371.0	332	-84
PLS14-203	598460.2	6390079.3	499.0	350.0	39	-90
PLS14-204	597929.0	6389869.0	499.0	299.0	320	-90
PLS14-205	598636.2	6390162.6	499.0	421.0	85	-90
PLS14-207	598529.2	6390032.9	499.0	455.0	341	-81
PLS14-208	599283.9	6390477.4	499.0	407.0	171	-90
PLS14-209	598281.3	6390002.2	499.0	272.0	331	-82
PLS14-210	598397.3	6390033.5	499.0	299.0	341	-81
PLS14-211	598610.9	6390146.6	499.0	413.0	168	-90
PLS14-213	598581.2	6390061.5	499.0	311.0	336	-81
PLS14-214	598404.0	6390059.1	499.0	413.0	40	-90
PLS14-215	598427.1	6390040.8	499.0	299.0	331	-80
PLS14-216	598462.2	6390036.7	499.0	347.0	335	-84
PLS14-217	598365.1	6390035.1	499.0	320.0	336	-77
PLS14-218	598264.1	6389929.3	499.0	287.0	328	-71
PLS14-219	598086.3	6389924.1	499.0	327.0	337	-90
PLS14-220	598300.2	6390031.8	499.0	341.0	273	-90
PLS14-221	598520.1	6390016.3	499.0	317.0	328	-71
PLS14-222	598167.4	6389928.4	499.0	221.0	335	-69
PLS14-223	598295.8	6390041.4	499.0	308.4	305	-90
PLS14-224	598624.7	6390115.6	499.0	389.0	340	-71
PLS14-225	598609.1	6390038.6	499.0	329.0	325	-72
PLS14-226	598298.3	6389962.6	499.0	360.0	332	-70
PLS14-227	598433.2	6389989.1	499.0	317.0	325	-72
PLS14-228	598424.9	6390046.0	499.0	527.0	198	-90
PLS14-229	598122.9	6389915.3	499.0	248.0	338	-71
PLS14-230	598678.9	6390102.9	499.0	420.0	333	-71
PLS14-231	598195.2	6389969.7	499.0	275.0	337	-72
PLS14-232	598090.1	6389877.1	500.0	345.0	336	-70
PLS14-233	598390.0	6389977.9	499.0	344.0	337	-71
PLS14-235	598320.3	6390017.3	499.0	302.3	309	-70
PLS14-236	598709.8	6390145.9	499.0	407.0	338	-70
PLS14-237	598618.3	6390128.3	499.0	378.0	336	-70
PLS14-238	598616.0	6390022.3	499.0	431.0	332	-71
PLS14-240	598421.1	6390017.6	499.0	326.0	337	-72
PLS14-241	598078.0	6389905.4	499.0	323.0	329	-71
PLS14-242	598647.5	6390064.4	499.0	395.0	342	-69
PLS14-243	598277.5	6389972.0	499.0	356.0	333	-71
PLS14-244	598425.2	6390047.0	499.0	275.0	335	-70

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS14-246	598454.7	6390049.9	499.0	316.0	336	-70
PLS14-247	598303.9	6389989.0	499.0	374.0	333	-70
PLS14-248	598601.5	6390054.0	499.0	452.0	321	-70
PLS14-250	598107.4	6389946.8	499.0	294.0	330	-69
PLS14-253	598508.4	6390045.8	499.0	338.0	352	-72
PLS14-254	598610.6	6390147.5	499.0	407.0	336	-70
PLS14-256	598298.1	6389999.4	499.0	338.0	336	-70
PLS14-257	598727.4	6390102.8	499.0	476.0	332	-68
PLS14-259	598615.9	6390058.7	499.0	431.9	335	-69
PLS14-261	598271.4	6389988.1	499.0	302.0	337	-69
PLS14-263	598810.8	6390138.3	499.0	398.0	333	-69
PLS14-264	598869.8	6390194.2	499.0	392.0	335	-69
PLS14-266	598538.8	6390087.3	499.0	353.0	342	-72
PLS14-267	598696.4	6390060.9	499.0	374.0	334	-72
PLS14-270	598064.4	6389898.7	499.0	374.0	336	-70
PLS14-271	598284.9	6389993.7	499.0	335.0	334	-69
PLS14-273	598648.0	6390093.6	499.0	452.0	332	-70
PLS14-274	598875.1	6390179.2	499.0	417.0	340	-68
PLS14-275	598751.5	6390159.8	499.0	434.0	333	-69
PLS14-276	598340.0	6390014.5	499.0	338.0	337	-70
PLS14-278	598585.5	6390089.9	499.0	344.0	332	-69
PLS14-279	598488.0	6390017.6	499.0	371.0	337	-70
PLS14-282	598630.0	6390138.0	499.0	569.0	339	-71
PLS14-283	598621.1	6390045.6	499.0	389.0	336	-70
PLS14-285	598856.3	6390143.6	499.0	500.0	347	-70
PLS14-286	598266.6	6389997.1	499.0	293.0	335	-71
PLS14-287	598636.1	6390048.6	499.0	413.0	336	-70
PLS14-289	598048.9	6389891.8	499.0	347.0	336	-70
PLS14-290	598473.7	6390122.7	499.0	452.0	156	-70
PLS14-293	598623.5	6390080.8	499.0	383.0	334	-70
PLS14-294	598295.0	6390007.4	499.0	356.0	333	-70
PLS14-296	598618.9	6390236.7	499.0	494.0	156	-70
PLS14-297	598644.7	6390255.5	499.0	476.0	156	-71
PLS14-298	598635.2	6390018.9	499.0	389.0	332	-70
PLS15-299	598249.9	6389993.7	499.4	263.0	336	-72
PLS15-300	598769.9	6390155.1	499.0	395.0	336	-72
PLS15-301	598642.0	6390113.1	499.0	371.0	336	-71
PLS15-302	598501.9	6390016.8	499.1	281.0	336	-71
PLS15-303	598237.8	6389987.1	499.0	200.0	335	-70
PLS15-304	598888.0	6390221.1	498.6	383.0	336	-70
PLS15-308	598382.8	6390027.8	499.0	314.0	336	-70
PLS15-311	598246.8	6390003.2	499.1	206.0	336	-73

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS15-312	598765.9	6390164.9	499.0	380.0	336	-72
PLS15-315	598242.0	6389977.7	499.0	227.0	336	-70
PLS15-318	598291.1	6390016.2	499.0	332.0	336	-70
PLS15-319	598924.1	6390216.0	499.0	407.0	336	-71
PLS15-321	598224.2	6389981.0	499.0	251.4	336	-71
PLS15-324	598792.0	6390176.9	499.0	425.0	336	-71
PLS15-325	598507.0	6390008.0	499.1	336.0	336	-70
PLS15-327	598920.1	6390224.9	499.0	308.0	336	-71
PLS15-328	597987.9	6389774.9	499.0	431.0	336	-75
PLS15-330	598761.6	6390174.7	499.0	386.0	336	-71
PLS15-332	597860.9	6389839.0	499.1	254.0	336	-70
PLS15-333	597729.3	6389802.7	508.9	332.0	336	-69
PLS15-334	598261.9	6390007.1	499.1	260.0	336	-71
PLS15-337	598821.4	6390187.8	499.1	407.0	336	-70
PLS15-339	597754.0	6389857.2	509.4	227.0	336	-71
PLS15-341	598786.9	6390186.1	499.1	353.0	336	-72
PLS15-343	597225.1	6389607.2	541.2	368.0	336	-69
PLS15-344	598758.1	6390183.0	499.0	434.0	336	-70
PLS15-346	597225.1	6389607.1	541.3	366.5	335	-77
PLS15-348	598842.9	6390214.1	499.1	341.0	336	-71
PLS15-351	598688.0	6390233.9	499.0	407.0	156	-79
PLS15-352	597219.0	6389622.0	541.3	272.0	340	-74
PLS15-353	598491.0	6390008.1	499.0	370.0	336	-72
PLS15-354	598928.1	6390206.0	499.1	407.0	336	-71
PLS15-355	598699.9	6390239.1	499.0	344.0	156	-78
PLS15-356	598009.9	6389728.5	499.0	349.3	344	-61
PLS15-357	599259.9	6390419.9	499.1	330.0	336	-70
PLS15-358	598602.0	6390165.9	499.0	350.0	336	-71
PLS15-359	598849.0	6390200.0	499.0	347.0	336	-71
PLS15-360	597250.1	6389625.1	542.1	257.5	336	-69
PLS15-361	598983.0	6390230.0	499.1	353.0	336	-70
PLS15-362	598545.1	6389996.0	499.1	467.0	336	-76
PLS15-363	598645.9	6390028.3	499.1	359.0	336	-69
PLS15-364	597200.8	6389624.1	541.6	251.0	333	-79
PLS15-365	598613.0	6390103.0	499.1	401.0	336	-70
PLS15-366	598594.9	6390180.2	499.1	284.0	336	-70
PLS15-367	597187.7	6389618.1	541.7	260.0	331	-79
PLS15-368	598255.0	6389985.0	499.1	293.0	336	-73
PLS15-369	598640.9	6390075.2	499.1	410.0	336	-71
PLS15-370	598636.8	6390123.0	499.0	350.0	336	-71
PLS15-371	598102.0	6389924.2	499.1	320.9	336	-71
PLS15-372	597243.0	6389641.2	542.0	371.0	331	-78

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS15-373	598388.1	6390054.0	499.2	356.0	155	-87
PLS15-374	598217.0	6389961.0	499.1	275.0	336	-73
PLS15-375	598258.8	6389976.1	499.1	281.0	336	-72
PLS15-376	598105.6	6389914.4	499.1	323.0	336	-70
PLS15-377	598233.0	6389962.2	499.1	246.7	336	-70
PLS15-378	598655.1	6390120.0	499.0	387.4	336	-71
PLS15-379	598313.8	6389995.3	499.1	332.0	336	-72
PLS15-380	598088.0	6389918.0	499.0	335.0	336	-72
PLS15-381	598728.0	6390139.2	499.2	380.0	336	-72
PLS15-382	598277.9	6390009.1	499.1	281.0	336	-69
PLS15-383	598655.9	6390081.2	499.1	414.0	336	-71
PLS15-384	598247.9	6389965.0	499.1	230.0	336	-69
PLS15-385	598758.9	6390144.1	499.0	373.0	336	-71
PLS15-386	598598.9	6390098.1	499.1	341.0	336	-70
PLS15-387	598221.5	6389952.0	498.9	257.0	336	-72
PLS15-388	598818.9	6390119.8	498.9	431.0	336	-70
PLS15-389	597226.8	6389640.2	540.6	402.0	334	-80
PLS15-391	598263.0	6389965.0	499.0	80.0	336	-70
PLS15-391A	598265.0	6389965.2	498.9	296.0	343	-70
PLS15-392	598069.0	6389889.0	499.0	101.0	330	-72
PLS15-392A	598069.4	6389887.7	498.9	374.0	332	-69
PLS15-393	598875.1	6390178.5	498.9	395.0	339	-72
PLS15-394	599303.8	6390432.6	498.8	320.0	330	-71
PLS15-395	597174.0	6389612.1	543.1	192.1	338	-79
PLS15-397	598319.2	6389984.6	499.0	356.0	344	-72
PLS15-398	597184.4	6389626.9	541.5	430.2	335	-79
PLS15-399	598824.7	6390104.0	498.9	392.0	328	-70
PLS15-400	599298.2	6390445.9	498.9	278.0	339	-69
PLS15-402	598330.8	6390002.0	498.7	362.0	337	-73
PLS15-403	598110.8	6389905.6	498.9	335.0	335	-71
PLS15-404	597254.8	6389650.2	541.6	399.1	334	-80
PLS15-405	599310.9	6390416.7	498.8	357.0	332	-70
PLS15-408	597161.2	6389606.3	544.3	266.0	337	-79
PLS15-409	598235.4	6389956.3	498.9	290.0	335	-70
PLS15-410	598126.6	6389909.5	498.9	311.0	336	-72
PLS15-411	597197.1	6389633.1	541.1	434.0	336	-80
PLS15-413	599290.2	6390426.5	498.9	299.0	334	-70
PLS15-414	598090.4	6389910.7	498.9	326.0	324	-72
PLS15-416	598883.2	6390162.7	498.8	419.0	333	-69
PLS15-417	598073.4	6389879.9	498.9	343.0	334	-71
PLS15-418	597143.7	6389603.6	544.2	431.0	336	-81
PLS15-423	597268.8	6389656.1	540.2	441.0	334	-80

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS15-426	597170.2	6389621.1	543.5	416.0	336	-79
PLS15-427	598863.7	6390157.3	498.8	419.0	335	-71
PLS15-428	597259.8	6389640.1	541.6	410.0	337	-81
PLS15-431	598903.4	6390153.1	498.8	431.0	330	-72
PLS15-432	597234.0	6389663.2	540.8	371.0	334	-80
PLS15-434	597157.2	6389614.1	543.9	423.5	336	-79
PLS15-435	598896.2	6390168.0	498.8	437.0	338	-71
PLS15-436	597221.1	6389647.3	540.5	420.6	332	-79
PLS15-438	597205.0	6389615.1	541.1	401.0	334	-80
PLS15-439	597211.0	6389640.2	541.1	374.3	334	-80
PLS15-440	598874.3	6390141.2	498.8	396.9	328	-73
PLS15-441	597192.4	6389608.1	541.8	413.0	336	-81
PLS15-442	597132.0	6389594.0	542.9	404.0	334	-80
PLS15-443	597265.1	6389626.2	541.7	446.0	337	-80
PLS15-444	597141.3	6389611.5	544.1	419.0	334	-80
PLS16-445	597037.7	6389475.2	547.4	317.0	336	-81
PLS16-446	597148.0	6389593.2	544.3	368.0	336	-82
PLS16-447	597207.1	6389647.2	541.0	357.0	333	-81
PLS16-449	597175.3	6389611.0	543.4	407.0	337	-81
PLS16-450	597263.9	6389665.0	540.3	410.0	332	-81
PLS16-451	597135.9	6389585.2	543.6	272.0	333	-81
PLS16-452	598143.4	6389942.7	498.9	278.0	331	-73
PLS16-454	597193.1	6389646.0	541.3	395.0	333	-82
PLS16-455	598290.0	6389985.8	498.9	350.0	338	-70
PLS16-456	597260.2	6389674.1	540.6	329.0	338	-80
PLS16-458	598838.2	6390151.9	498.9	431.0	337	-72
PLS16-459	599131.1	6390266.7	498.9	359.0	333	-71
PLS16-460	599177.2	6390426.1	499.1	273.0	132	-90
PLS16-462	597040.8	6389470.8	548.7	317.0	335	-79
PLS16-463	598835.3	6390157.4	498.9	383.3	336	-72
PLS16-464	599175.8	6390391.3	498.9	218.0	337	-71
PLS16-465	597030.0	6389459.1	548.1	302.0	337	-81
PLS16-466	599083.3	6390379.2	498.9	296.0	291	-90
PLS16-468	599162.1	6390386.1	498.8	224.7	334	-71
PLS16-470	597056.9	6389471.3	546.9	317.0	338	-80
PLS16-471	598862.3	6390158.4	499.0	389.0	337	-71
PLS16-473	597034.9	6389482.1	547.4	311.0	334	-81
PLS16-474	599084.2	6390376.0	498.9	221.0	337	-71
PLS16-475	598888.7	6390184.6	498.9	401.0	335	-72
PLS16-476	596976.4	6389430.7	547.5	335.0	338	-80
PLS16-479	596939.8	6389401.9	546.6	360.3	339	-80
PLS16-481	599204.9	6390400.1	498.9	221.0	336	-70

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS16-483	597051.1	6389485.1	547.3	335.0	332	-80
PLS16-484	596972.1	6389440.1	547.9	302.0	333	-81
PLS16-485	599202.4	6390408.2	499.0	239.0	338	-72
PLS16-487	599179.5	6390381.8	499.1	209.0	334	-74
PLS16-488	596946.1	6389389.0	547.6	362.0	335	-80
PLS16-489	599143.5	6390391.7	499.0	221.0	322	-71
PLS16-491	596937.0	6389409.1	546.8	344.0	334	-80
PLS16-493	597002.1	6389448.8	548.8	350.0	332	-80
PLS16-494	599115.8	6390377.8	499.0	221.0	329	-72
PLS16-495	597025.5	6389467.4	547.8	342.0	329	-81
PLS16-496	599172.2	6390398.5	499.0	215.0	329	-72
PLS16-498	599198.0	6390417.7	499.0	224.1	333	-73
PLS16-499	597288.1	6389691.2	539.6	456.0	331	-81
PLS16-500	599232.2	6390413.3	499.0	257.7	338	-70
PLS16-501	597021.1	6389478.3	547.6	308.0	338	-81
PLS16-502	596996.9	6389459.2	548.9	315.8	336	-80
PLS16-503	598522.8	6390121.0	499.0	845.0	155	-83
PLS16-504	596979.9	6389423.5	548.2	371.0	336	-81
PLS16-505	596915.7	6389378.7	546.7	337.0	336	-80
PLS16-506	597048.5	6389491.2	547.2	275.5	334	-81
PLS16-507	596913.0	6389387.9	547.2	344.0	336	-81
PLS16-508	597071.1	6389513.2	548.7	267.9	337	-81
PLS16-510	596896.9	6389351.9	546.1	305.0	336	-80
PLS16-512	597090.0	6389543.0	547.4	305.0	337	-81
PLS17-513	599157.0	6390395.1	498.9	218.3	337	-70
PLS17-515	597094.8	6389534.5	547.8	314.0	337	-79
PLS17-516	599146.9	6390382.2	499.0	266.0	332	-71
PLS17-517	597086.8	6389552.0	547.8	311.0	339	-79
PLS17-518	599168.0	6390408.2	498.9	227.0	338	-74
PLS17-520	599192.5	6390427.3	498.9	236.0	335	-75
PLS17-521	597075.9	6389504.0	547.9	298.3	333	-80
PLS17-522	599166.0	6390377.2	498.8	230.0	334	-71
PLS17-524	597066.9	6389521.7	548.9	293.0	330	-80
PLS17-525	599184.0	6390371.9	498.9	302.0	336	-72
PLS17-526	597106.0	6389582.6	544.3	293.0	334	-80
PLS17-527	599228.0	6390422.3	498.9	233.0	334	-70
PLS17-528	599235.9	6390403.1	498.9	261.2	333	-71
PLS17-529	597110.0	6389573.0	544.1	305.0	334	-81
PLS17-530	596427.1	6389242.4	554.2	291.0	159	-89
PLS17-531	599257.0	6390430.1	499.0	258.0	334	-70
PLS17-533	596441.1	6389232.2	554.1	264.0	337	-81
PLS17-534	599253.1	6390438.9	499.0	245.0	333	-70

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS17-536	598946.1	6390314.9	498.9	533.0	154	-81
PLS17-537	596438.1	6389240.2	554.3	204.8	331	-80
PLS17-539	596411.8	6389223.0	553.0	329.0	333	-79
PLS17-541	597114.8	6389563.0	544.2	350.0	335	-82
PLS17-542	598939.9	6390328.9	498.9	374.0	157	-80
PLS17-545	597083.0	6389560.6	548.1	278.0	335	-80
PLS17-546	598861.2	6390324.6	499.0	215.0	330	-70
PLS17-547	596407.5	6389232.8	553.0	317.0	338	-80
PLS17-548	597098.2	6389523.9	547.1	311.0	333	-81
PLS17-551	597079.4	6389493.8	547.3	320.8	335	-80
PLS17-553	596416.7	6389211.0	552.4	296.0	337	-80
PLS17-557	596403.3	6389205.7	551.5	302.0	340	-80
PLS17-560	596387.9	6389203.0	551.2	302.0	333	-81
PLS17-561	596422.4	6389202.4	551.5	332.0	343	-81
PLS17-562	596392.3	6389193.6	551.2	308.0	335	-80
PLS17-563	596425.9	6389193.0	551.4	383.0	332	-81
PLS17-564	596396.8	6389183.7	550.2	328.0	339	-78
PLS17-565	596364.1	6389185.0	550.5	151.0	331	-80
PLS17-566	596400.9	6389173.9	550.0	335.0	342	-79
PLS17-567	596367.9	6389175.9	549.5	361.0	338	-79
PLS17-568	596405.0	6389164.6	549.6	428.0	333	-80
PLS17-MET-C	598418.3	6390053.9	498.9	258.0	318	-90
PLS17-MET-E	598618.5	6390056.8	498.9	329.0	325	-68
PLS17-MET-W	598109.2	6389957.2	499.0	224.0	155	-89
PLS18-569	596407.6	6389196.9	551.0	383.0	329	-82
PLS18-570	596382.0	6389180.4	550.2	335.0	337	-81
PLS18-571	596385.5	6389172.2	549.9	350.0	333	-79
PLS18-572	596410.9	6389187.1	550.6	401.0	332	-82
PLS18-573	598285.8	6389991.1	498.9	323.0	333	-72
PLS18-574	596389.1	6389162.9	549.4	350.0	336	-79
PLS18-575	598501.1	6390027.2	498.9	335.0	335	-71
PLS18-576	596393.0	6389153.0	549.1	338.0	331	-80
PLS18-577	596413.8	6389180.0	550.6	416.0	340	-83
PLS18-578	596433.1	6389213.4	552.7	113.0	330	-81
PLS18-578A	596433.4	6389212.5	552.9	305.0	335	-80
PLS18-579	598329.9	6390005.7	498.9	317.0	334	-68
PLS18-580	598596.9	6390063.2	499.0	317.0	337	-69
PLS18-581	598533.4	6390027.6	498.9	308.0	335	-69
PLS18-582	598358.0	6390015.1	499.0	314.6	333	-69
PLS18-583	598576.5	6390149.5	499.0	407.0	155	-70
PLS18-584	598566.6	6390144.1	499.1	335.9	155	-70
PLS18-585	598338.4	6389982.0	499.0	320.0	331	-71

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS18-586	598267.1	6390058.5	499.0	329.0	153	-69
PLS18-587	598247.4	6390057.6	499.0	250.0	154	-70
PLS18-588	598433.4	6390003.1	498.9	317.0	333	-69
PLS18-589	598453.2	6390006.7	498.9	299.0	332	-70
PLS18-590	598334.5	6389987.9	499.0	335.0	330	-70
PLS18-591	598326.3	6389990.3	499.0	335.0	332	-68
PLS21-592	598879.0	6390170.2	499.2	101.0	334	-66
PLS21-592A	598879.9	6390168.6	499.2	287.0	335	-67
PLS21-593	598815.9	6390130.0	499.2	356.0	335	-67
PLS21-594	598840.6	6390186.1	499.2	281.0	337	-70
PLS21-595	598823.9	6390108.9	499.2	353.0	337	-69
PLS21-596	598846.8	6390170.9	499.2	338.0	337	-70
PLS21-597	598670.1	6390089.5	499.2	383.0	335	-70
PLS21-598	598834.9	6390162.1	499.2	359.0	337	-68
PLS21-599	598829.9	6390168.3	499.2	326.0	340	-71
PLS21-600	598674.1	6390079.1	499.2	374.0	337	-70
PLS21-601	598682.8	6390093.8	499.2	377.0	336	-70
PLS21-602	598706.3	6390080.7	499.2	382.0	337	-70
PLS21-603	598687.4	6390082.7	499.2	362.0	339	-70
PLS21-604	598683.0	6390057.9	499.2	374.0	337	-70
PLS21-605	598701.9	6390090.1	499.2	389.0	335	-68
PLS21-606	598666.0	6390098.0	499.2	371.0	336	-69
PLS21-607	598814.7	6390169.9	499.2	344.0	339	-76
PLS21-608	598678.5	6390069.9	499.2	363.8	336	-70
PLS21-609	598878.3	6390180.5	499.2	329.0	337	-75
PLS21-610	598694.8	6390068.8	499.2	365.0	334	-70
PLS21-611	598852.2	6390160.0	499.2	332.0	341	-70
PLS21-612	597043.9	6389388.0	543.9	281.0	336	-61
PLS21-613	597046.5	6389381.4	543.8	286.0	337	-61
PLS21-614	597022.1	6389363.3	546.3	290.0	337	-60
PLS21-615	597017.4	6389374.9	546.7	254.0	340	-63
PLS21-616	596982.2	6389380.9	548.2	248.0	341	-73
PLS21-617	597006.0	6389438.9	548.9	269.0	337	-79
PLS21-618	597101.9	6389486.2	546.3	242.8	335	-70
PLS21-619	597031.3	6389566.8	545.2	251.0	157	-72
PLS21-620	597174.0	6389576.1	544.0	200.0	335	-71
PLS21-621	597070.9	6389478.0	546.8	230.0	335	-72
PLS21-622	597149.5	6389558.4	544.5	224.0	337	-72
PLS21-623	597125.8	6389534.1	544.7	224.0	284	-72
PLS21-624	597209.1	6389609.2	541.3	200.0	350	-72
PLS21-625	597099.9	6389482.9	546.4	213.7	336	-60
PLS21-626	597088.9	6389507.9	547.4	215.0	335	-71

Hole ID	Easting (UTM NAD83)	Northing (UTM NAD83)	Elevation (MASL)	Depth (m)	Azimuth (degrees)	Dip (degrees)
PLS21-627	597079.4	6389494.0	546.7	251.0	350	-72
PLS21-628	597074.6	6389468.6	546.7	224.0	335	-71
PLS21-629	597025.2	6389432.9	548.2	224.0	335	-71
PLS21-630	596966.0	6389380.7	548.0	227.0	336	-73
PLS21-631	596969.4	6389372.8	548.1	264.0	336	-72
PLS21-632	597069.7	6389331.8	537.3	352.0	336	-52
PLS21-633	596978.3	6389389.4	547.8	263.0	338	-73
PLS21-634	597069.8	6389627.8	543.8	221.0	156	-71
PLS21-635	597073.9	6389618.8	544.0	248.3	157	-71
PLS21-636	597076.7	6389613.1	544.1	221.0	156	-72
PLS21-MET-001	597060.6	6389522.5	549.2	200.0	218	-90
PLS21-MET-002	597079.8	6389565.2	548.0	200.0	54	-90
PLS21-MET-003	597149.7	6389624.7	543.9	161.0	321	-89
PLS21-MET-004	597207.4	6389654.0	540.8	161.0	271	-90
PLS22-CP-005	596384.4	6389212.4	551.6	180.5	287	-89
PLS24-652	596448.3	6389139.5	553.0	302.0	337	-65
PLS24-653	596377.5	6389189.7	549.4	335.0	338	-80
PLS24-655	596398.6	6389211.7	550.3	302.0	335	-81
PLS24-656	596393.3	6389194.4	549.9	302.0	335	-80
PLS24-658	596454.0	6389125.3	552.9	320.0	336	-65
PLS24-659	596429.4	6389114.5	552.9	350.0	336	-65
PLS24-660	596407.6	6389116.0	552.2	365.4	337	-67
PLS24-662	596459.7	6389113.5	552.8	359.0	336	-65
PLS24-663	596447.8	6389171.3	551.7	281.0	336	-65
PLS24-664	596421.7	6389130.7	552.6	332.0	336	-66
PLS24-665	596437.2	6389124.3	553.0	345.0	336	-66
PLS24-666	596444.1	6389178.9	551.7	278.0	335	-65
PLS24-668	596453.8	6389157.5	552.0	278.0	336	-65
PLS24-669	596443.5	6389109.7	552.9	377.0	338	-65
PLS24-671	596411.2	6389108.3	552.5	323.0	336	-62
PLS24-673	596375.5	6389193.8	549.6	284.0	336	-78
PLS24-675	596434.3	6389168.0	551.4	304.3	337	-65
PLS24-676	596392.5	6389193.1	549.9	293.0	337	-75
PLS24-677	596395.3	6389218.5	550.6	290.0	335	-81
PLS21-RM-003	596934.9	6389540.2	545.5	275.0	130	-69
PLS21-RM-002	597150.0	6389700.2	543.2	245.0	180	-71
PLS21-RM-001	597023.5	6389429.4	548.1	254.0	0	-74
PLS19-PW-08	598393.6	6390008.4	499.1	341.0	329	-71
PLS19-PW-09	598521.1	6390029.4	499.0	320.0	336	-69
PLS19-PW-10	598745.2	6390141.6	498.9	372.5	338	-70