

Exceptional Metallurgical Recoveries Open up Material Near Term Heap Leach Cashflow Opportunity from Van Uden Gold Project

Highlights

- Column leach testwork on Laterite gold mineralisation delivers exceptional recoveries of 88% after a very short 35 day leaching period
- These rapid leaching characteristics were achieved on all Laterite samples tested providing confidence of metallurgical performance across the mineralisation
- Agglomeration achieved at a very coarse 25mm crush
- These exceptional results provide a significant, near term cashflow opportunity in treating near or at surface gold bearing Laterite via a heap leach operation on site
- Current Laterite Resource that could be initially utilized in the heap leach operation is 1.05 Mt @ 0.52 g/t Au for 17,700 ounces*
- The Company also expects 1.85 Mt @ 1.05 g/t au for 62,400 ounces** in transition material may also be amenable to heap leach.
- Engineering and design studies underway to assess financial metrics
- With a simple 'free dig' mining to access ore, along with high recoveries from a simple short leach, the Company expects a very low capital and operating cost operation
- Mining proposal to be lodged under the EMA rapid approval framework
- The Company estimates study outcomes to be concluded in Q2 2026 and a Final Investment Decision to be made in Q3

TG Metals Limited (**TG Metals** or the **Company**) (ASX:TG6) is pleased to provide initial results from column leach metallurgical testwork underway for the Laterite material of the Van Uden Gold Project in Western Australia.

TG Metals CEO, Mr. David Selfe stated;

"These initial results from the column leach testwork are exceptional and give us a high level of confidence of favourable outcomes for a heap leaching operation on over one million tonnes of Laterite within the Van Uden gold deposit (see Table 1).

Achieving 88% gold extraction after 35 days is a remarkable result. The use of an on site heap leaching technology to recover gold from the Laterite resource is a low risk option to monetise

* See Table 1 ** See Table 2

the lower grade Laterite ores, enabling a more efficient exploitation of the entire mineral resource at Van Uden.

The Laterite is at surface, so requires no pre-stripping, minimal handling and a potential onsite facility means no transport costs. This delivers low mining costs, coupled with the low upfront capital and operating costs associated with heap leach processing.

We also expect the transitional zones of the Van Uden resource will be amenable to the same process and metallurgical testwork on this mineralisation type will be undertaken.

The final recoveries will be provided when the full leach cycle is completed, anticipated to be another 3 weeks under leach. The metallurgical testwork will be used to design and engineer suitable heap leach infrastructure for onsite installation and progress mining proposals.”

Gold Heap Leach Rationale

The Laterite resources at Van Uden are well suited to onsite heap leaching as evidenced by the rapid gold recoveries seen in the testwork and the exceptional physical characteristics. Being at surface and with no waste removal required for extraction, the Laterite presents a low cost mining opportunity. Onsite processing eliminates trucking costs and milling costs associated with toll milling and ore purchase to third party processing plants.

Whilst there is higher grade Laterite available at Van Uden such as the 12,496 tonnes @ 2.55g/t Au identified in ASX release 21 August 2025 which is suitable to be toll milled offsite, the majority of the Laterite resources are at a lower grade which is more suitable for onsite heap leaching. The current Laterite resource for the Van Uden project has a high proportion within the Indicated category available for mine design. **Table 1** below summarises the Laterite resource and **Figure 2** shows the grade distribution of the Laterite resource.

Table 1: Van Uden Laterite Resource (Subset of the Van Uden MRE – see Table 5)

Material	Indicated			Inferred			Total		
	Tonnes	Grade (Au g/t)	Gold (oz)	Tonnes	Grade (Au g/t)	Gold (oz)	Tonnes	Grade (Au g/t)	Gold (oz)
Laterite	886,000	0.56	15,900	167,000	0.33	1,800	1,053,000	0.52	17,700

The heap leaching process also allows for much lower cut-off grades as the processing cost is far less than that of a conventional carbon in leach (CIL) plant. Capital costs are also lower. These low capital and operating costs combine to enable the exploitation of the entire Laterite resource available. Whilst the full results from the column leach testwork are completing, mining and processing studies have commenced to determine the optimal mining and pad design parameters.

A focus on early cashflow, to capitalise on the rapid leaching characteristics, will be a key feature of the mining and processing studies currently underway.

Rapid leaching times will enable turnover of leach pads in weeks rather than months. The turnover time will dictate production rates.

Existing Infrastructure

The Van Uden site has already established an all-weather haul road, water bore and storage and site facilities. A Mining Proposal will be applied for to commence mining the Laterite, construct heap leach pads, ponds, crushing and agglomeration facilities. The water requirements should be satisfied by onsite extraction in place. It is anticipated that the Laterite heap leach project will qualify as an Eligible Mining Activity (EMA) under the guidelines introduced in September 2025 by the DMPE which will allow rapid approvals (target approval 46 days) for low-risk activities. Laterite resources are located on granted Mining Leases.

Additional Heap Leach Opportunities

The Van Uden resource contains a significant proportion of transition material which may be suitable for the application of heap leach technology. The physical characteristics of transition material lends itself to agglomeration more readily than oxide or fresh material types. The Company intends to conduct heap leach testwork on transition material as soon as sufficient sample for agglomeration and column leach testwork is available. As the transition material sits below the oxide and above the fresh material in the resource, it would need to be accessed as part of the larger ultimate pit mining scenario. **Figure 1** shows the transition zone in the northern part of the Van Uden resource. The current transition material defined is shown in **Table 2** below.

Table 2: Van Uden Transition Resource (Subset of the Van Uden MRE – see Table 5)

Material	Indicated			Inferred			Total		
	Tonnes	Grade (Au g/t)	Gold (oz)	Tonnes	Grade (Au g/t)	Gold (oz)	Tonnes	Grade (Au g/t)	Gold (oz)
Transition	1,115,000	1.07	38,300	740,000	1.01	24,100	1,855,000	1.05	62,400

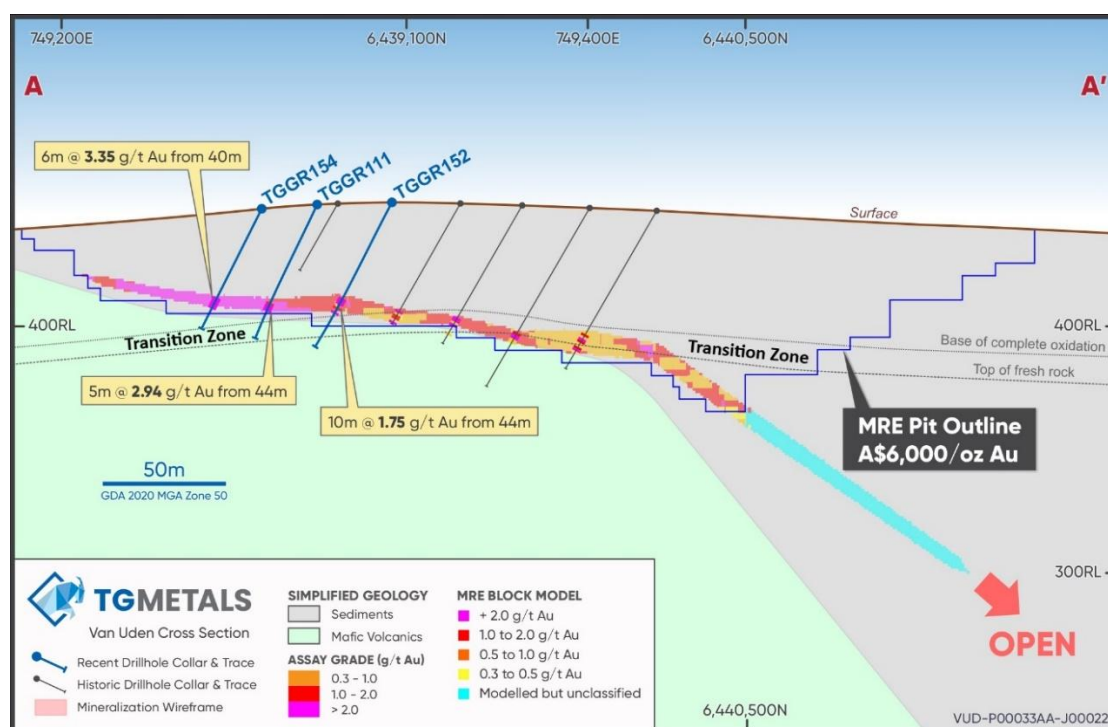
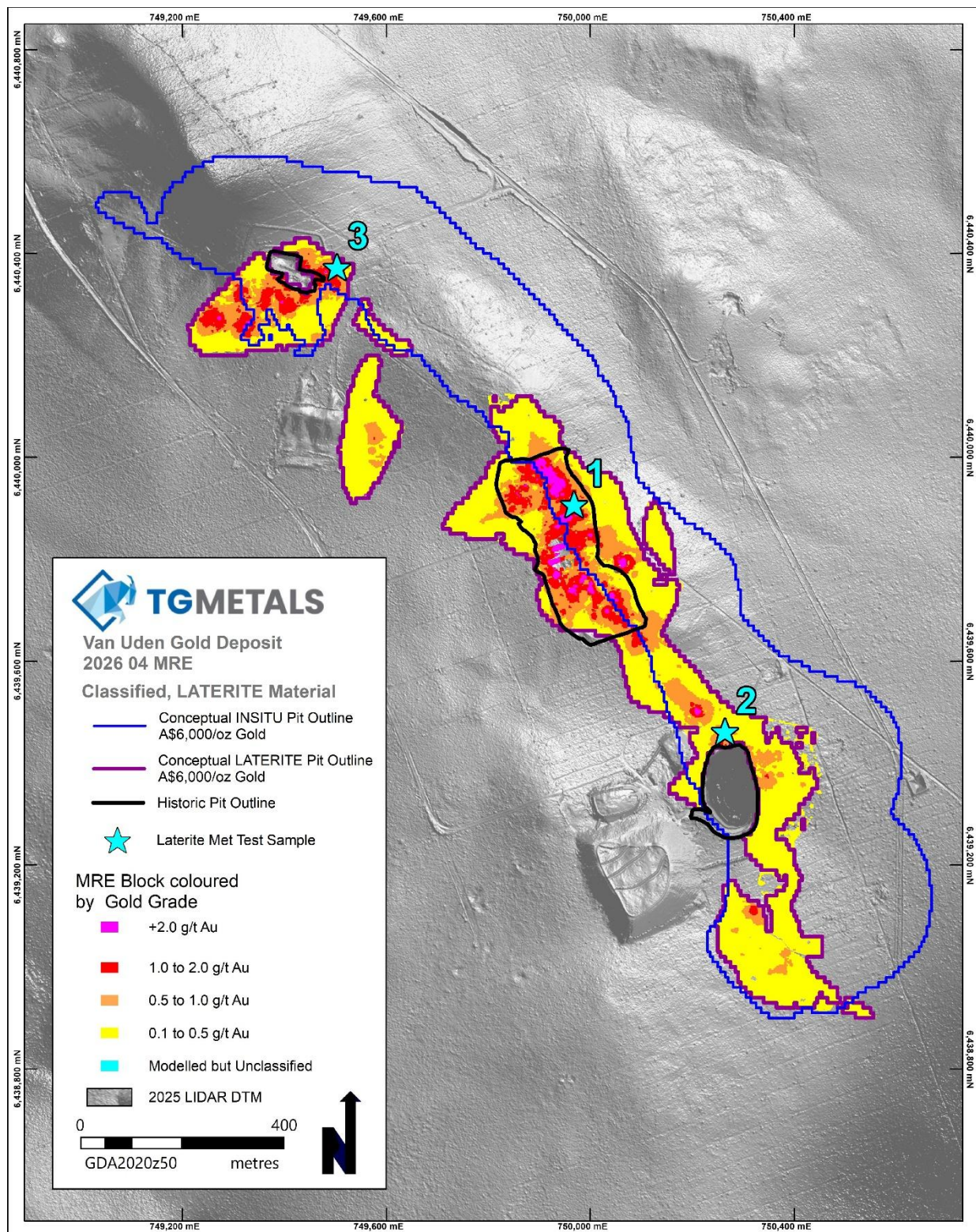


Figure 1 – Cross section showing the transition zone in the northern end of the Van Uden resource



Gold Leaching Testwork Overview

TG Metals has engaged Independent Metallurgical Operations Pty Ltd (IMO) based in Western Australia, to conduct column leach metallurgical testwork on lateritic samples recovered from previous mining stockpiles and historical surface excavations at the Company's Van Uden Gold project. The testwork is ongoing at Metallurgy Pty Ltd, a commercial laboratory located in Perth, Western Australia. The results and testwork program were overseen by independent consultant Michael Rodriguez.

This testwork is primarily to determine the amenability of the auriferous Laterite mineralisation to conventional cyanide heap leach processing.

A total of three (3) composites were generated utilising samples taken from historical mine workings which have exposed Laterite. **Figure 2** shows the location of the samples and **Table 3** lists the location coordinates.

Table 3 – Collar Locations of Metallurgical Samples

Sample ID	Type	Easting	Northing	Tenement No.
L01	Composite	749,968.22	6,439,909.94	M77/477
L02	Composite	750,264.15	6,439,464.67	M77/478
L03	Composite	749,503.00	6,440,375.34	M77/477

Each sample is a set of composite samples taken from exposures at historical mining disturbances. Samples were selected based on lithology type, being pisolitic Laterite which has been shown to have favourable physical properties for the application of heap leach extraction methods.

These samples first underwent intermittent bottle roll (IBR) tests to determine initial suitability to cyanide leaching under non-grind conditions, see **Table 4** for these results.

Table 4 – IBR Results for Samples 1, 2 and 3

Composite		Laterite Pit - Column 1			Tasman - Column 2			Dieman - Column 3		
Leach Test	#	IBR-04	IBR-05	IBR-06	IBR-07	IBR-08	IBR-09	IBR-10	IBR-11	IBR-12
Crush Size	mm	25	12.5	8	25	12.5	8	25	12.5	8
Calculated Ore Head Grade	g/t	0.29	0.19	0.18	0.23	0.22	0.22	0.40	0.39	0.34
Assay Ore Head Grade	g/t	0.15	0.15	0.15	0.21	0.21	0.21	0.36	0.36	0.36
Head SxS Ore Head Grade	g/t	0.15	0.15	0.14	0.21	0.21	0.21	0.44	0.44	0.44
0 Hour Au Recovery	%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%	0.0%
2 Hour Au Recovery	%	10.5%	21.6%	27.5%	47.8%	49.3%	53.6%	10.0%	5.1%	5.8%
4 Hour Au Recovery	%	21.0%	37.9%	33.1%	56.8%	58.6%	58.3%	12.6%	7.7%	14.6%
8 Hour Au Recovery	%	24.6%	43.0%	49.5%	67.0%	67.8%	71.9%	12.7%	15.5%	23.5%
24 Hour Au Recovery	%	35.2%	48.6%	60.4%	65.3%	68.1%	68.0%	27.8%	33.4%	46.8%
48 Hour Au Recovery	%	49.2%	59.5%	60.9%	77.9%	81.6%	72.5%	35.5%	38.7%	61.6%
72 Hour Au Recovery	%	42.7%	60.0%	66.7%	78.3%	82.0%	81.6%	43.2%	49.0%	62.1%
96 Hour Au Recovery	%	48.0%	70.9%	77.8%	74.2%	88.6%	77.2%	46.0%	49.4%	62.5%
168 Hour Au Recovery	%	61.9%	81.4%	88.5%	78.3%	91.0%	90.5%	53.8%	62.2%	72.6%
240 Hour Au Recovery	%	91.3%	81.8%	88.7%	91.2%	91.7%	82.5%	61.8%	72.9%	68.0%
Leach Residue Grade	g/t	0.02	0.03	0.02	0.02	0.02	0.04	0.15	0.10	0.11
Overall Gold Recovery	g/t	0.26	0.15	0.16	0.21	0.20	0.18	0.24	0.28	0.26
Total NaCN Cons	kg/t	1.19	0.91	1.16	1.27	1.19	1.17	0.72	0.89	0.97
Total Lime Cons	kg/t	2.87	3.04	3.00	2.64	2.59	2.58	3.93	4.16	4.15

The composite samples were then tested to determine optimal parameters for agglomeration.

The intermittent bottle roll testwork results are aligned to the heap leach results to date. An important consideration when progressing column heap leaching testwork. The 25mm crush size performed the best of the three crush sizes tested, being 25mm, 12.5mm and 8mm. These results suggest the gold is primarily located outside of the pisolites rather than internal which should aid cyanide penetration. This is also reinforced with a consistently low residue grade which suggests that the majority of the gold is exposed to the cyanide leach agent. IBR tests achieved +91% gold recovery on the preferred 25mm crush size.

Figure 3 below shows an example of Sample 2 agglomerates prior to and as loaded in the test column.



Figure 3 - Column two leach agglomerates on the left and inside the column on the right

Prior to loading the columns, further tests were performed on the agglomerates to determine indicative percolation rates. The results of these tests were used to determine the cement addition rate for agglomeration and the initial cyanide solution feed rate. The agglomeration was achieved with a 15kg/tonne cement addition to the 25mm crushed Laterite feed.

The column heights tested are at 4 metres and 2 metres and the column tests are performed sequentially. **Figure 4** shows columns one and two (both 4m in height) and column 3 (2m in height). The third, 2 metre high column will test for variation in leach kinetics with height and also for visual observations within the column, as the 2m column is a clear tube.

All columns are currently under leach, when recoveries of gold slow sufficiently to determine completion, the leaching will terminate and the agglomerate residue will be analysed for final recoveries.

To determine ongoing recoveries, carbon is added to the recovered leach solution weekly to absorb the gold in solution (carbon loading). It is then removed for assay and initial determination of leach kinetics.



Figure 4 - Columns One, Two and Three Under Leach

Key initial findings are that only 2.94% slumping has been observed in column one, 13.9% in column two and 0.77% in column three. The leach kinetics are rapid in the initial time phases, achieving **88.0% recovery** in column two **after 35 days** and 67.7% recovery in column one after 42 days and 26.5% recovery in column three after 10 days following carbon loading. All columns remain under leach and are showing continuing gold extractions. The intended full leach time was up to 90 days for each column, however all will likely terminate early due to the rapid extractions seen so far.

At the end of this cycle the residue will be assayed and a final head grade and recovery calculated. Results may alter slightly from these preliminary results however rapid leaching and recovery is likely to remain evident. In addition, leachate addition rates, reagents use and water use will be calculated and used to determine optimum leach pad configurations and operational parameters for a Laterite heap leach operation on site. **Figures 5, 6 and 7** below show the graphical results to date.

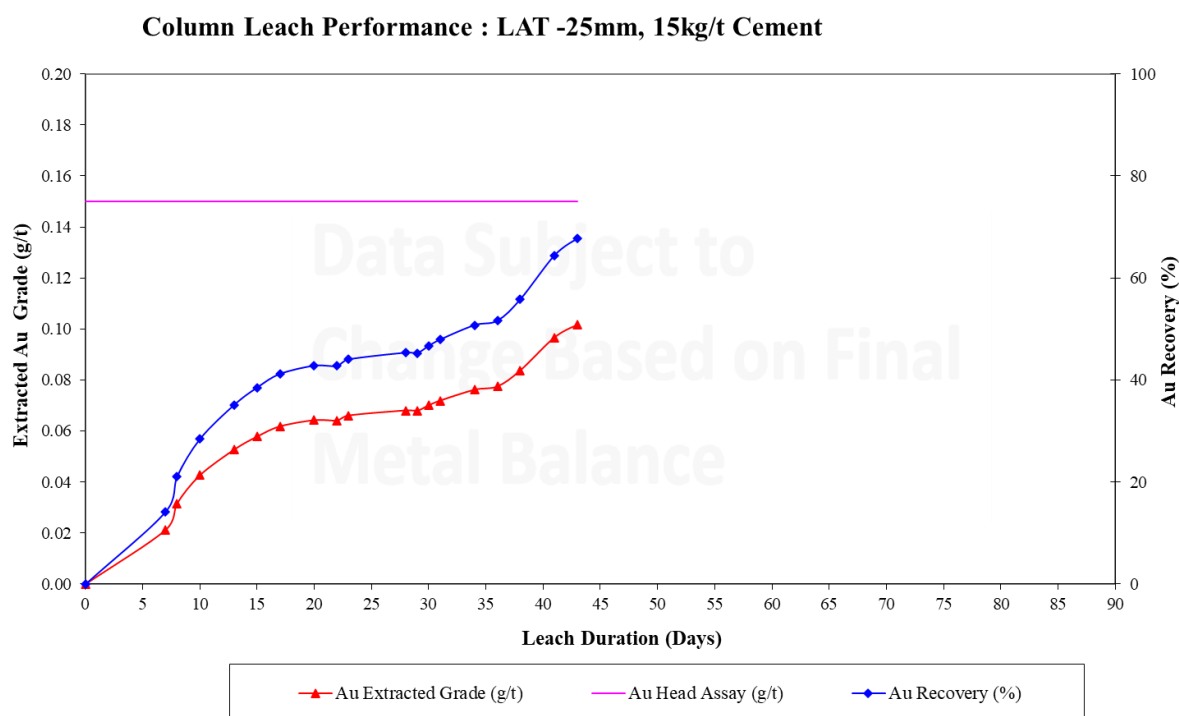


Figure 5 - Leaching Times for Column One Leach Tests

Column Leach Performance : TAS -25mm, 15kg/t Cement

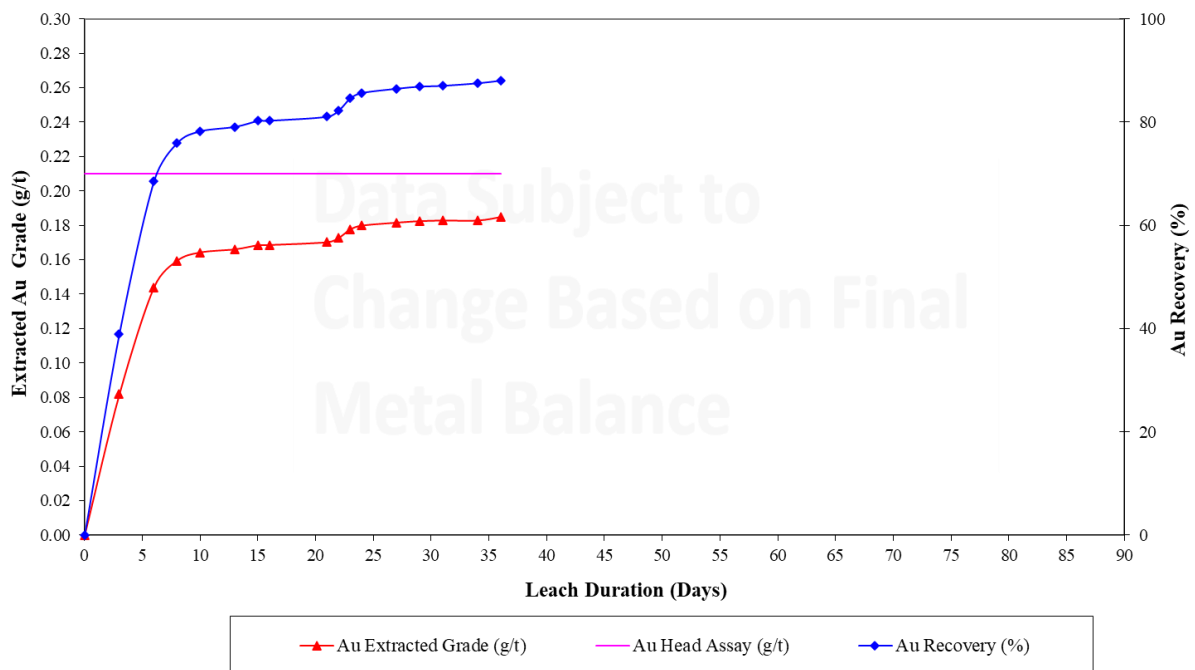


Figure 6 - Leaching Times for **Column Two** Leach Tests

Column Leach Performance : DBS -25mm, 15kg/t Cement

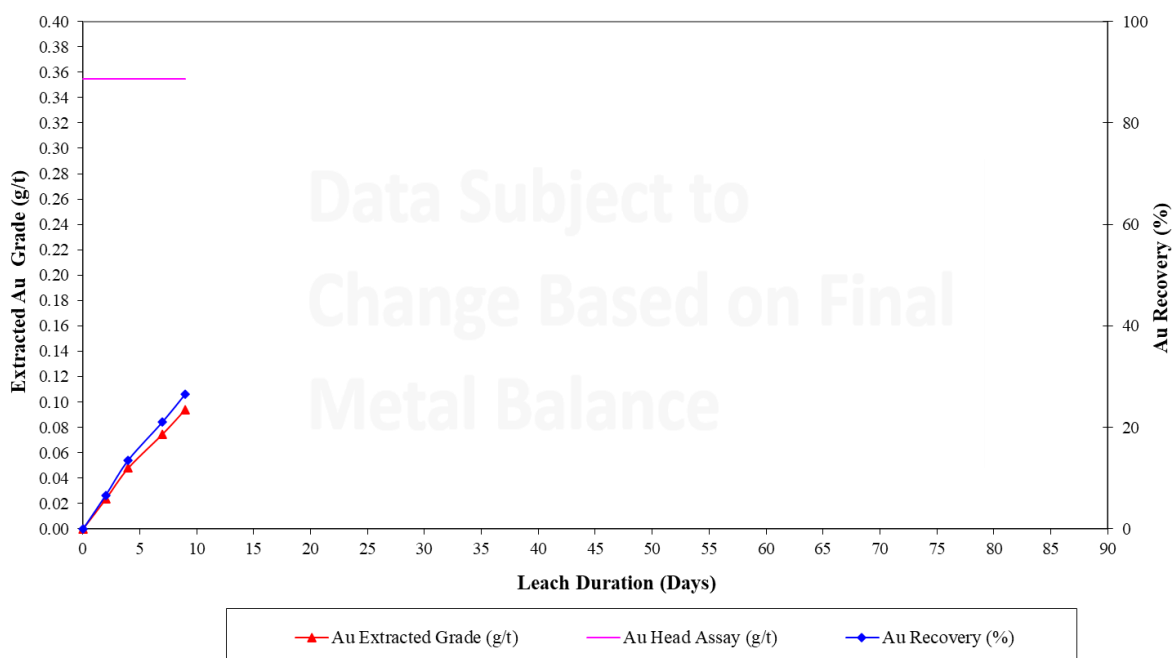


Figure 7 - Leaching Times for **Column Three** Leach Tests

Next Steps

- All three Columns under leach will progress and be monitored and recorded up to a full leach cycle.
- Commence application for a Mining Proposal to encompass Laterite mining and heap leach pads and facilities. Final pad design parameters will be determined from the full column leach test results which will be available at the end of the full leach cycle.
- The full metallurgical report will be made available to potential heap leach plant suppliers.
- Further optimisation testwork is planned to test the Laterite for improvements in reagent use and operating cost reductions via research and development initiatives.
- First stage grade control drilling of the Laterite will commence upon staged pit designs being finalised.
- Column leach testwork on other mineralisation types at Van Uden to also commence.

About the Van Uden Resource

The Van Uden gold MRE was updated earlier this month, increasing the Indicated category by more than 120%. This has allowed progression of mining and processing studies focused on utilising the Indicated resources in the near term. The surface Laterite is one component of this and the most immediate potential, however further Indicated resources deeper in the profile may also lend themselves to Heap Leach processing technology. The updated MRE below in **Table 5** shows the current resource status:

Table 5: MRE – Van Uden Gold Deposit

Mineral Resource Estimate Van Uden Gold Deposit - April 2026									
Material	Indicated			Inferred			Total		
	Tonnes	Grade (Au g/t)	Gold (oz)	Tonnes	Grade (Au g/t)	Gold (oz)	Tonnes	Grade (Au g/t)	Gold (oz)
Laterite	886,000	0.56	15,900	167,000	0.33	1,800	1,053,000	0.52	17,700
Oxide	1,976,000	1.15	73,300	414,000	0.91	12,100	2,390,000	1.11	85,400
Transition	1,115,000	1.07	38,300	740,000	1.01	24,100	1,855,000	1.05	62,400
Fresh	580,000	1.35	25,100	2,057,000	1.21	80,200	2,637,000	1.24	105,300
Total	4,557,000	1.04	152,600	3,378,000	1.09	118,200	7,935,000	1.06	270,800

NOTES: The Mineral Resources statement conforms to the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves (JORC Code) 2012 Edition. All tonnages are dry metric tonnes. The laterite portion of the mineralisation has been reported at a cut-off grade of 0.10 g/t Au by area within a A\$6,000/oz Au optimised pit shell. All other material types are reported at a cut-off grade of 0.30 g/t Au by area within a A\$6,000/oz Au optimised pit shell based on mining parameters and operating costs typical for Australian open pit extraction deposits of a similar scale and geology.

Minor discrepancies may occur due to rounding of appropriate significant figures. The resources comply with the Reasonable Prospects for Eventual Economic Extraction (RPEEE), a key principle in mineral resource reporting that requires the competent person to demonstrate that a mineral deposit has the potential to be economically extracted in the future.

About TG Metals

TG Metals is an ASX listed company focused on exploring and developing gold and lithium assets at its wholly owned Lake Johnston Project and 80% owned Van Uden Gold Project in the stable jurisdiction of Western Australia. The Lake Johnston Project hosts the Burmeister high grade lithium deposit, Jaegermeister lithium pegmatites and several surrounding lithium prospects. Burmeister is in proximity to four lithium processing plants and undeveloped deposits. The Van Uden Gold Project contains past producing gold mines and is in proximity to operating gold processing Plants (Figure 8).

Authorised for release by TG Metals Board of Directors.

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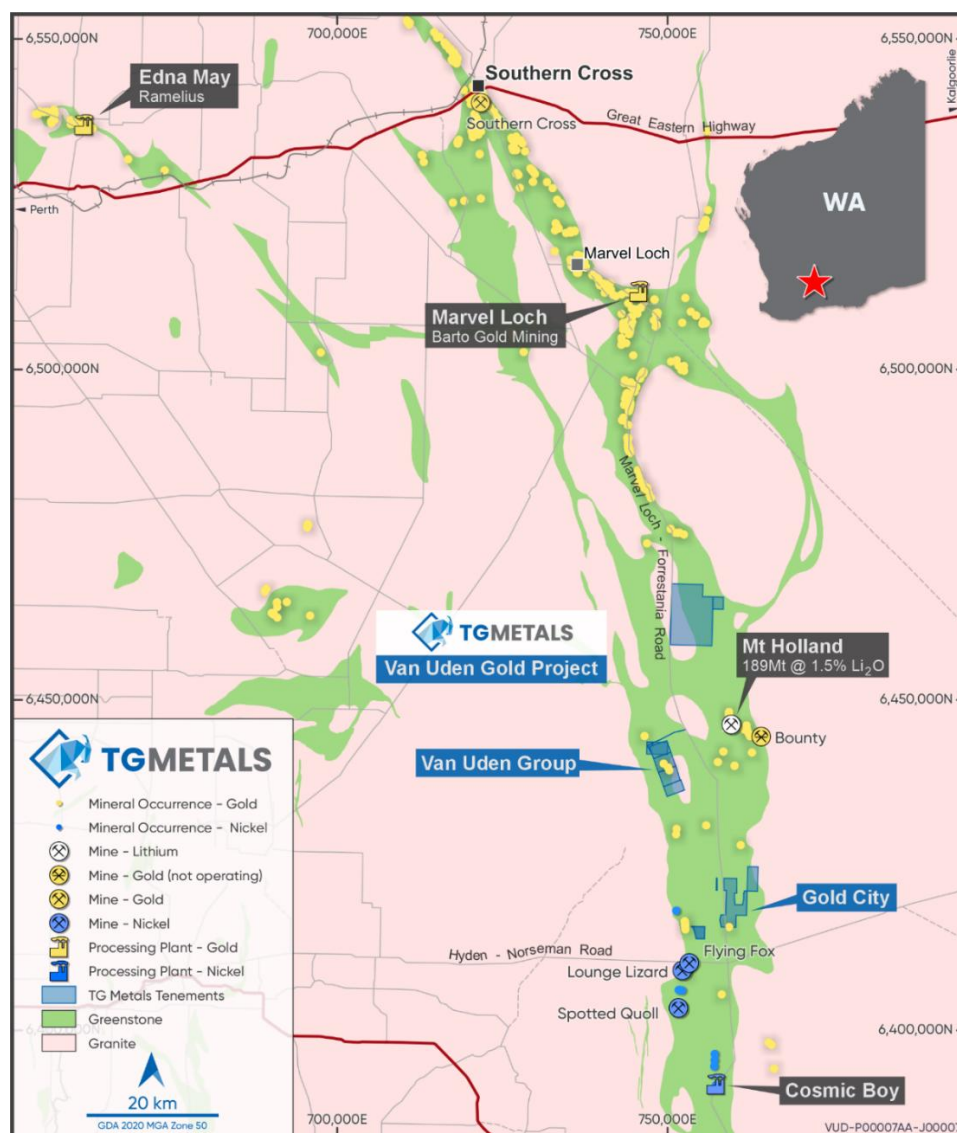


Figure 8 – Location Map showing TG Metals' Van Uden Gold Project



Competent Person Statement

Information in this announcement that relates to exploration results, exploration strategy, exploration targets, geology, drilling and mineralisation is based on information compiled by Mr David Selfe who is a Fellow of the Australasian Institute of Mining and Metallurgy. Mr Selfe has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activities that he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. Mr Selfe has consented to the inclusion in this report of matters based on their information in the form and context in which it appears.

Information in this announcement that relates to metallurgical results, is based on information compiled by Mr David Selfe and has been reviewed by Mr Michael Rodriguez who is a Fellow of the Australasian Institute of Mining and Metallurgy. Mr Rodriguez has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activities that he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the Australasian Code for Reporting of Metallurgical Results. Mr Rodriguez has consented to the inclusion in this report of matters based on their information in the form and context in which it appears.

Forward Looking Statements

This announcement may contain certain statements that may constitute “forward looking statements”. Such statements are only predictions and are subject to inherent risks and uncertainties, which could cause actual values, results, performance achievements to differ materially from those expressed, implied or projected in any forward looking statements.

Forward-looking statements are statements that are not historical facts. Words such as “expect(s)”, “feel(s)”, “believe(s)”, “will”, “may”, “anticipate(s)” and similar expressions are intended to identify forward-looking statements. These statements include, but are not limited to statements regarding future production, resources or reserves and exploration results. All such statements are subject to certain risks and uncertainties, many of which are difficult to predict and generally beyond the control of the Company, that could cause actual results to differ materially from those expressed in, or implied or projected by, the forward-looking information and statements. These risks and uncertainties include, but are not limited to: (i) those relating to the interpretation of drill results, the geology, grade and continuity of mineral deposits and conclusions of economic evaluations, (ii) risks relating to possible variations in reserves, grade, planned mining dilution and ore loss, or recovery rates and changes in project parameters as plans continue to be refined, (iii) the potential for delays in exploration or development activities or the completion of feasibility studies, (iv) risks related to commodity price and foreign exchange rate fluctuations, (v) risks related to failure to obtain adequate financing on a timely basis and on acceptable terms or delays in obtaining governmental approvals or in the completion of development or construction activities, and (vi) other risks and uncertainties related to the Company's prospects, properties and business strategy. Our audience is cautioned not to place undue reliance on these forward-looking statements that speak only as of the date hereof, and we do not undertake any obligation to revise and disseminate forward-looking statements to reflect events or circumstances after the date hereof, or to reflect the occurrence of or non-occurrence of any events.

The Company believes that it has a reasonable basis for making the forward-looking Statements in the presentation based on the information contained in this and previous ASX announcements.

The Company is not aware of any new information or data that materially affects the information included in this ASX release, and the Company confirms that, to the best of its knowledge, all material assumptions and technical parameters underpinning the exploration results in this release continue to apply and have not materially changed.

JORC Code, 2012 Edition – Table 1

Section 1 Sampling Techniques and Data

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	- Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. - Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. - Aspects of the determination of mineralisation that are Material to the Public Report. - In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information.	Bulk samples were collected from laterite material exposed in historical workings and stockpiles within the Van Uden Project. Sampling comprised multiple grab samples collected across exposed pisolitic laterite zones. These were composited to generate bulk samples of sufficient mass for metallurgical testwork. In selected areas, sampling was undertaken proximal to known mineralisation to ensure adequate gold tenor for metallurgical assessment.
Drilling techniques	Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc).	No drilling was undertaken for this metallurgical testwork. Bulk samples were obtained from surface exposures and historical workings.
Drill sample recovery	- Method of recording and assessing core and chip sample recoveries and results assessed. - Measures taken to maximise sample recovery and ensure representative nature of the samples. - Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.	Not applicable.
Logging	Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical	Not applicable.

Criteria	JORC Code explanation	Commentary
	studies. • Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography. • The total length and percentage of the relevant intersections logged.	
Sub-sampling techniques and sample preparation	• If core, whether cut or sawn and whether quarter, half or all core taken. • If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry. • For all sample types, the nature, quality and appropriateness of the sample preparation technique. • Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples. • Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling. • Whether sample sizes are appropriate to the grain size of the material being sampled.	• Bulk samples recovered from 3 stockpiled mineralised ore were received, and homogenised. Each composite sample was staged crushed to 100% passing 25mm. Homogenised sub-samples were split out to produce 10kg, 20kg and 220kg charges. • The 20kg and 10kg homogenised composite sub-samples were crushed to 12.5mm and 8mm respectively in preparation for downstream testwork including intermittent bottle roll and column leach testwork.
Quality of assay data and laboratory tests	• The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. • For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc. • Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.	• Metallurgical testwork including intermittent bottle roll (IBR) and column leach tests was managed by Independent Metallurgical Operations Pty Ltd (IMO) staff, at Metallurgy Pty Ltd a commercial laboratory located in Western Australia. • A sizing analysis was completed on composite sub-samples. • All composite samples prepared for downstream testwork had ICP OES analysis for 42 elements completed and gold assays were determined using standard fire assay methods. • Raw water was recovered from the mine stie, assayed and used for all subsequent testwork. • Samples were recovered from the IBR tests and columns to obtain kinetic time vs extraction curves. IBR and column testwork was completed in parallel to obtain "read across" information. • Kappes drawdown tests were applied to establish optimum agglomeration operating conditions.

Criteria	JORC Code explanation	Commentary
		4m columns were predominantly used to reflect the forecast heap leach bench heights. A “clear” 2m column was used to observe the flow characteristics and for comparison in the leach cycle between a 4m column and a 2m column. - Metallurgical recoveries were calculated from solution assays and carbon loading estimates. Final recoveries will be reconciled with residues from the testwork.
Verification of sampling and assaying	- The verification of significant intersections by either independent or alternative company personnel. - The use of twinned holes. - Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols. - Discuss any adjustment to assay data.	Testwork procedures and results have been reviewed by an independent metallurgical consultant. The methods applied are considered appropriate for early-stage metallurgical assessment.
Location of data points	- Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. - Specification of the grid system used. - Quality and adequacy of topographic control.	- Coordinate system: MGA2020 Zone 50 for sample locations using GPS(+/- 3m accuracy). - Topography: LiDAR surface model.
Data spacing and distribution	- Data spacing for reporting of Exploration Results. - Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Ore Reserve estimation procedure(s) and classifications applied. - Whether sample compositing has been applied.	Sampling was selective and not conducted on a systematic grid. The sampling approach is not intended to represent spatial continuity, but rather to provide indicative metallurgical characteristics of laterite material types.
Orientation of data in relation to geological structure	- Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type. - If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.	Sampling was undertaken from surface exposures and is not considered to be biased by structural orientation.
Sample security	The measures taken to ensure sample security.	- Samples were sealed in 44 gallon drums or 20L sealed buckets and labelled at site. - Chain of custody; Samples were taken to Welshpool by TG Metals Limited personnel.

Criteria	JORC Code explanation	Commentary
<i>Audits or reviews</i>	<i>The results of any audits or reviews of sampling techniques and data.</i>	The metallurgical program and results have been reviewed by an independent metallurgical consultant..

Section 2 Reporting of Exploration Results

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
<i>Mineral tenement and land tenure status</i>	<i>Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings.</i> <i>The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.</i>	- All sampling is within in Mining Leases M77/477 and M77/478. The tenements are currently held by TG Gold Pty Ltd (80%) and Barto Gold Mining Pty Ltd (20%). Ownership: TG Metals Limited is the operator of the tenements via its 100% ownership of TG Gold Pty Ltd. - The tenements are in good standing and unaffected by heritage or environmental encumbrances.
<i>Exploration done by other parties</i>	<i>Acknowledgment and appraisal of exploration by other parties.</i>	- Dieman, Laterite and Tasman Pits were previously mined and drilled by earlier operators as part of historic gold extraction. - Historic data have been reviewed where available.
<i>Geology</i>	<i>Deposit type, geological setting and style of mineralisation.</i>	- Orogenic, shear- and vein-hosted gold mineralisation occurs within the Forrestania greenstone belt along the sediment–mafic contact, which is mapped as the Van Uden Shear. Host rocks are amphibolite-facies metasediments and mafic volcanic units showing local quartz veining and minor schistose alteration. Gold mineralisation is structurally controlled and consistent with regional orogenic systems of the Western Australian Yilgarn Craton. - Most gold mineralisation is formed within the sediments, however where the mafic/sediment contact undulates, the gold mineralisation is known to occur within the mafic rocks. - The laterite mineralisation comprises pisolitic and ferruginous material developed over primary gold mineralisation within the Van Uden Project area.

Criteria	JORC Code explanation	Commentary
<i>Drill hole Information</i>	• A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes: ○ easting and northing of the drill hole collar ○ elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar ○ dip and azimuth of the hole ○ down hole length and interception depth ○ hole length. • If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.	• No drilling results are reported in this announcement. This release relates to metallurgical testwork conducted on surface-derived composite samples.
<i>Data aggregation methods</i>	• In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated. • Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail. • The assumptions used for any reporting of metal equivalent values should be clearly stated.	• Metallurgical recoveries are reported based on calculated gold extraction derived from solution assays and carbon loading measurements over time. No grade aggregation or intercept compositing has been applied.
<i>Relationship between mineralisation widths and intercept lengths</i>	• These relationships are particularly important in the reporting of Exploration Results. • If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported. • If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg 'down hole length, true width not known').	• Not applicable
<i>Diagrams</i>	• Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.	• Relevant figures include sample locations, column leach setup and leach kinetics graphs are included in the body of the announcement.

Criteria	JORC Code explanation	Commentary
<i>Balanced reporting</i>	Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.	The announcement reports initial results from ongoing metallurgical testwork. Results are preliminary and final recoveries will be determined upon completion of the full leach cycle.
<i>Other substantive exploration data</i>	Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.	Metallurgical testwork includes bottle roll (IBR) and column leach tests on agglomerated laterite material. Test parameters include varying crush sizes and cement addition rates. Initial results indicate rapid leach kinetics and strong early gold recoveries. Samples are considered indicative only and not necessarily representative of the broader laterite mineralisation or expected mining feed.
<i>Further work</i>	- The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling). - Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.	- Ongoing metallurgical testwork will continue through the full column leach cycle to determine final recoveries and key operating parameters. Further optimisation testwork will assess reagent consumption and processing conditions to support future engineering and design studies. - Future heap leach testwork will focus on optimum bench height, irrigation rate and cycle time. - Saturation soil characterisation testwork will also be progressed to determine heap leach bench height stability confirmatory testwork. - Figure 2 in the body of the announcement shows the extent of laterite mineralisation which will be the focus of future drilling and extensions.